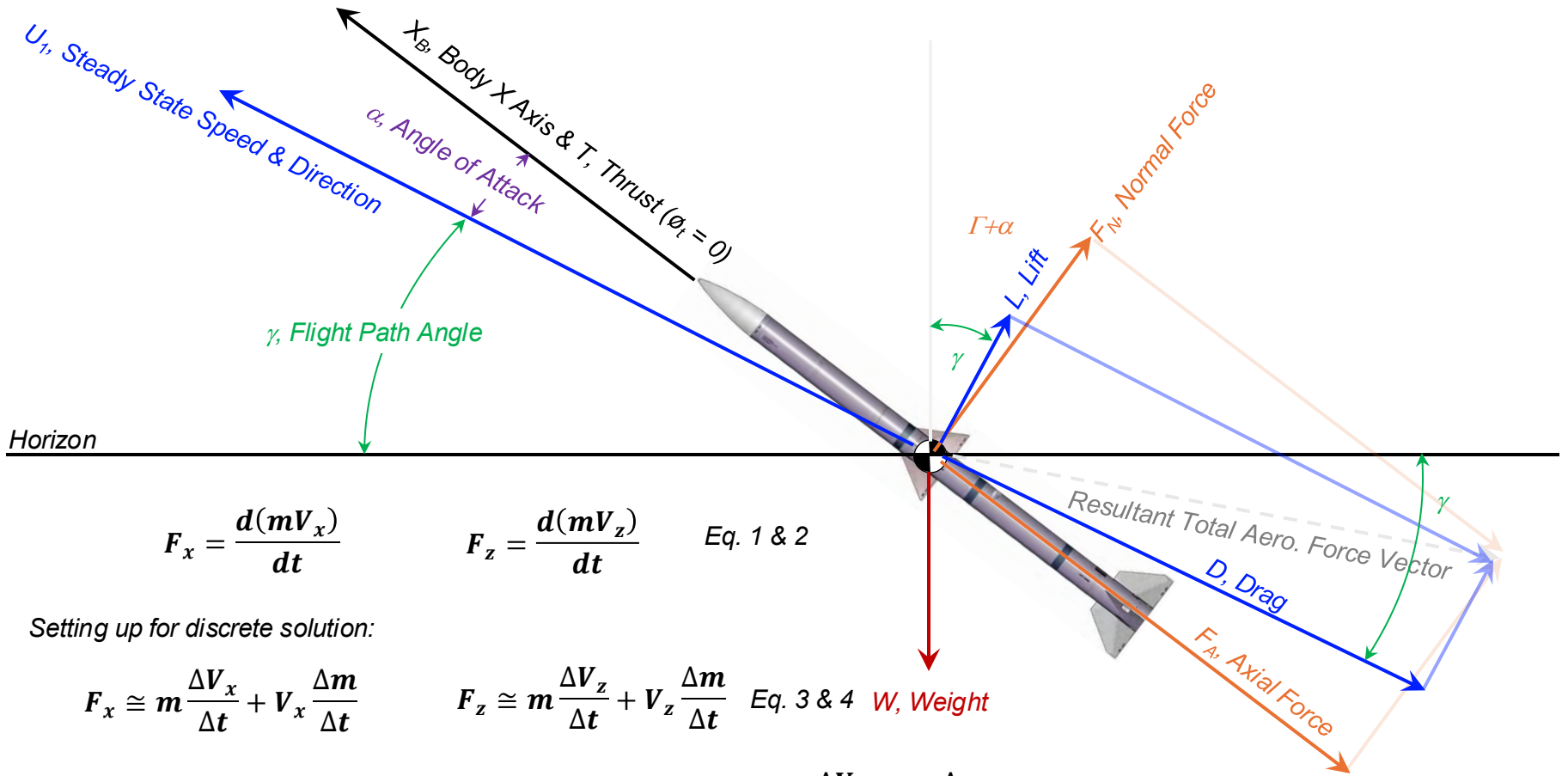


1st Order Proverse Engineering



$$F_x = \frac{d(mV_x)}{dt} \quad F_z = \frac{d(mV_z)}{dt} \quad \text{Eq. 1 \& 2}$$

Setting up for discrete solution:

$$F_x \cong m \frac{\Delta V_x}{\Delta t} + V_x \frac{\Delta m}{\Delta t} \quad F_z \cong m \frac{\Delta V_z}{\Delta t} + V_z \frac{\Delta m}{\Delta t} \quad \text{Eq. 3 \& 4}$$

$$F_x = T \cos(\alpha + \phi_t + \gamma) - C_D q A \cos \gamma - C_L q A \sin \gamma \cong m \frac{\Delta V_x}{\Delta t} + V_x \frac{\Delta m}{\Delta t}$$

$$F_z = T \sin(\alpha + \phi_t + \gamma) + C_L q A \cos \gamma - C_D q A \sin \gamma - W \cong m \frac{\Delta V_z}{\Delta t} + V_z \frac{\Delta m}{\Delta t} \quad \text{Eq. 6}$$

1st Order Proverse Engineering

Step 1: Get Launch Conditions: x_o , z_o coordinates, V_{x0} , V_{z0} , m_o , atmospherics

Note the velocities are often nonzero considering aircraft launch or tube launch from ground

Step 2: Find or determine information on powerplant: $T(t)$, $I_{sp}(t)$, $m_{propellant}$

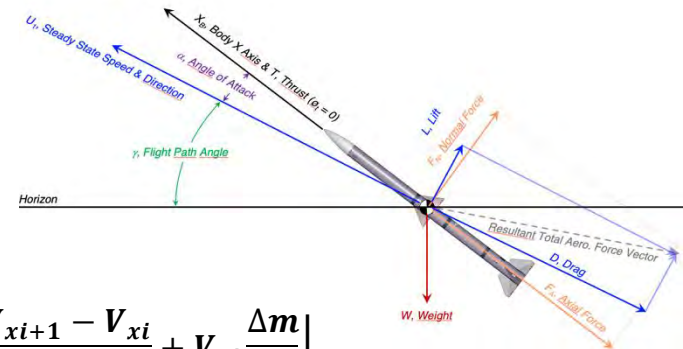
Step 3: Assume (initially) an angle of attack, α , and thrust angle, ϕ_t

Step 4: Solve for initial flight path angle, γ (from initial information)

Step 5: Break down equations 5 and 6 for discretization:

$$F_{xi} = T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \frac{V_{xi+1} - V_{xi}}{\Delta t} + V_{xi} \frac{\Delta m}{\Delta t} \Big|_i$$

$$F_{zi} = T_i \sin(\alpha_i + \phi_{ti} + \gamma_i) + C_{Li} q_i A \cos \gamma_i - C_{Di} q_i A \sin \gamma_i - W_i \cong m_i \frac{V_{zi+1} - V_{zi}}{\Delta t} + V_{zi} \frac{\Delta m}{\Delta t} \Big|_i$$



Step 6: Solve for x_{i+1} , z_{i+1} , m_{i+1} , V_{xi+1} , V_{zi+1} , V_{total} (U_1), q_{i+1} (using V_{total}), C_{Li+1} , C_{Di+1} , γ_{i+1}

Step 7: Adjust α_{i+1} , ϕ_{i+1} and T_{i+1} as needed

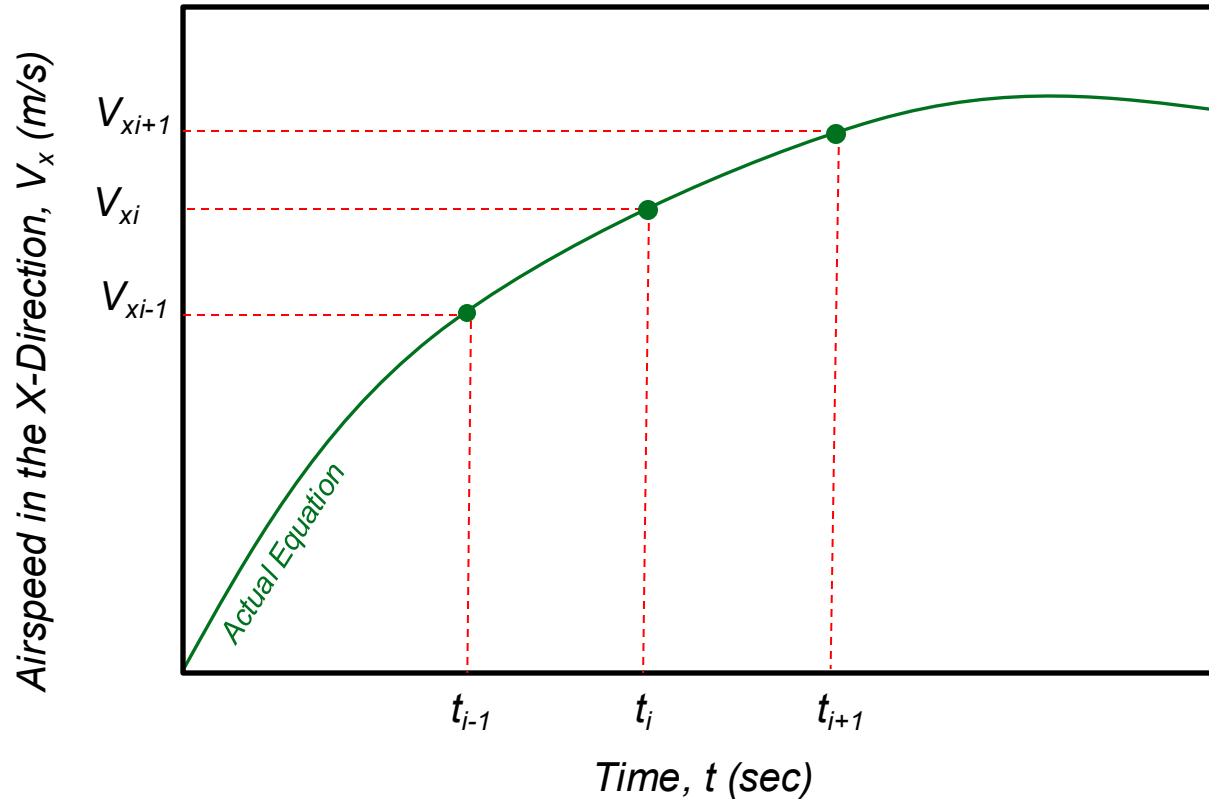
Step 8: Repeat

1st Order Proverse Engineering

Primer on Finite Difference Techniques & Numerical Solution

$$F_{xi} \cong T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left. \frac{\Delta V}{\Delta t} \right|_i + V_{xi} \left. \frac{\Delta m}{\Delta t} \right|_i$$

1st Order Difference Expression



1st Order Proverse Engineering

Primer on Finite Difference Techniques & Numerical Solution

$$F_{xi} \cong T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left. \frac{\Delta V}{\Delta t} \right|_i + V_{xi} \left. \frac{\Delta m}{\Delta t} \right|_i$$

Recall the Taylor Series Expansion:

$$f(x_{i+1}) = f(x_i) + \Delta x f'(x_i) + \frac{\Delta x^2}{2!} f''(x_i) + \frac{\Delta x^3}{3!} f'''(x_i) + \dots + \frac{\Delta x^n}{n!} f^n(x_i) + R_n$$

$$R_n = \frac{\Delta x^{n+1}}{n+1!} f^{(n+1)}(\xi)$$

1st Order Proverse Engineering

Primer on Finite Difference Techniques & Numerical Solution

$$F_{xi} \cong T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left. \frac{\Delta V}{\Delta t} \right|_i + V_{xi} \left. \frac{\Delta m}{\Delta t} \right|_i$$

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$$f(x_{i+1}) = f(x_i) + \Delta x f'(x_i) + \frac{\Delta x^2}{2!} f''(x_i) + \frac{\Delta x^3}{3!} f'''(x_i) + \dots + \frac{\Delta x^n}{n!} f^n(x_i) + R_n$$

$$R_n = \frac{\Delta x^{n+1}}{n+1!} f^{(n+1)}(\xi)$$

Use this to get an estimate for $f'(x_i)$: $f(x_{i+1}) = f(x_i) + \Delta x f'(x_i) + \frac{\Delta x^2}{2!} f''(x_i) + O(\Delta x^3)$ }

$$f'(x_i) = \frac{f(x_{i+1}) - f(x_i)}{\Delta x} - \frac{\Delta x}{2!} f''(x_i) + O(\Delta x^2)$$

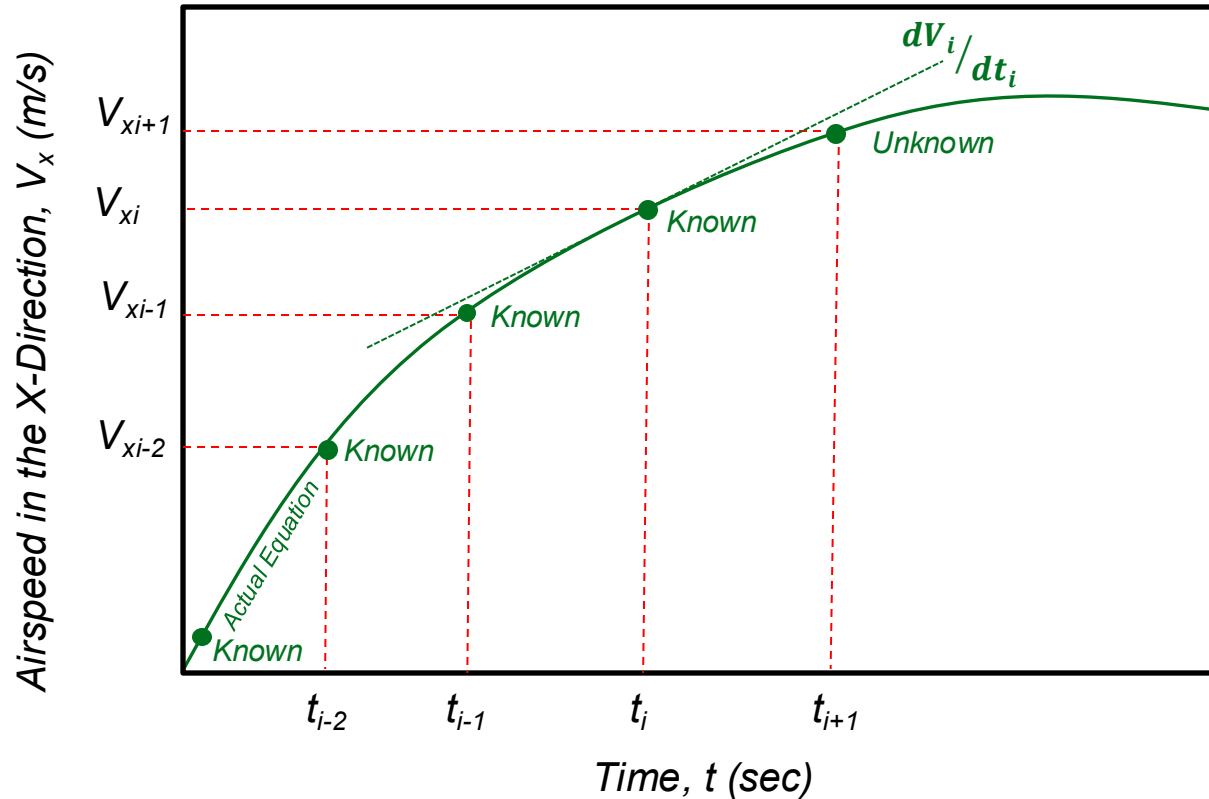
1st Order Proverse Engineering

Primer on Finite Difference Techniques & Numerical Solution

$$F_{xi} \cong T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left. \frac{\Delta V}{\Delta t} \right|_i + V_{xi} \left. \frac{\Delta m}{\Delta t} \right|_i$$

1st Order Difference Expression

$$\frac{dV}{dt} \cong \frac{\Delta V}{\Delta t}$$

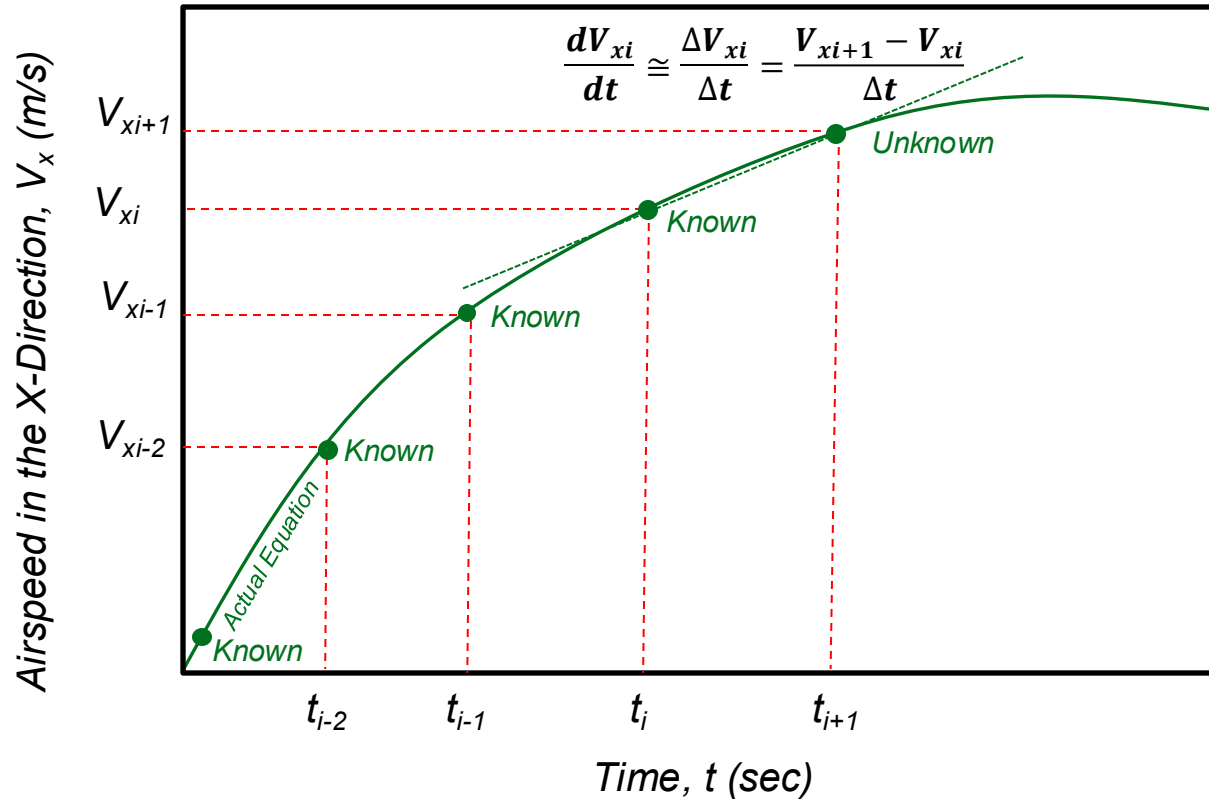


1st Order Proverse Engineering

Primer on Finite Difference Techniques & Numerical Solution

$$F_{xi} \cong T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left. \frac{\Delta V}{\Delta t} \right|_i + V_{xi} \left. \frac{\Delta m}{\Delta t} \right|_i$$

1st Order Forward Difference

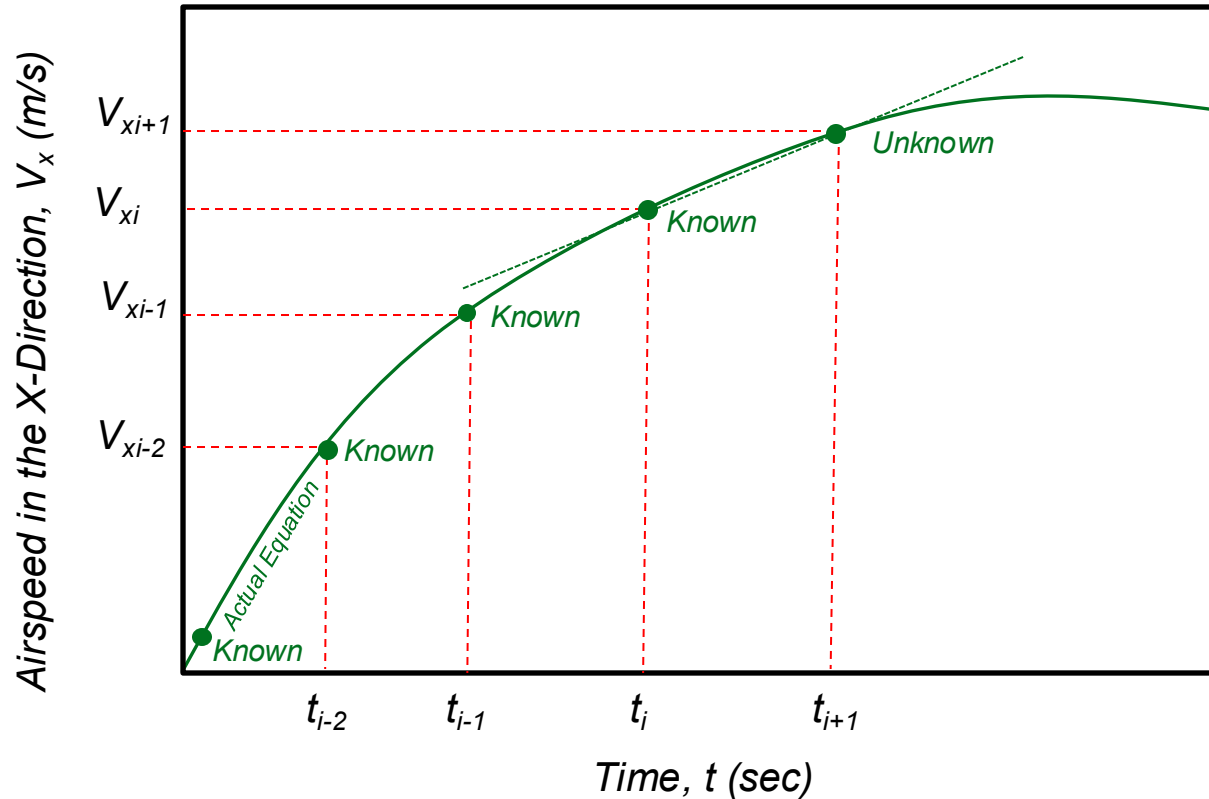


1st Order Proverse Engineering

Primer on Finite Difference Techniques & Numerical Solution

1st Order Forward Difference

$$\frac{dV_{xi}}{dt} \cong \frac{\Delta V_{xi}}{\Delta t} = \frac{V_{xi+1} - V_{xi}}{\Delta t}$$

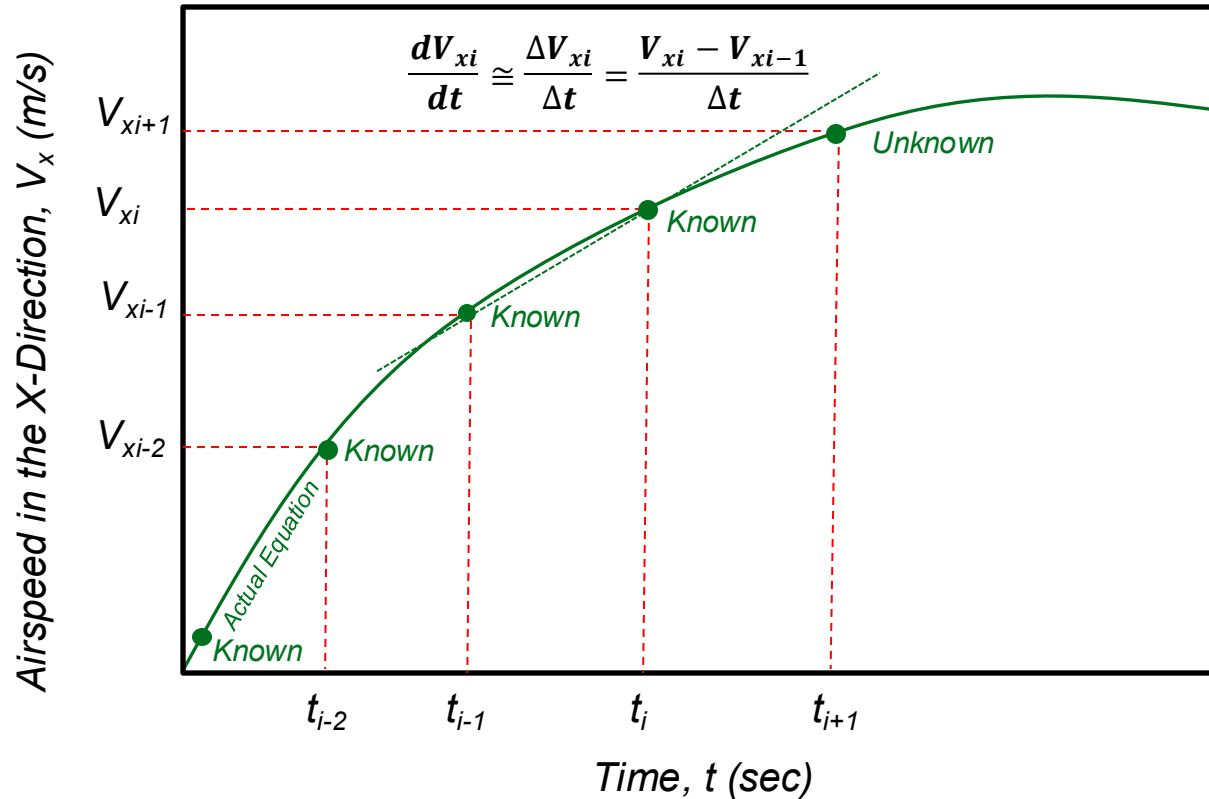


1st Order Proverse Engineering

Primer on Finite Difference Techniques & Numerical Solution

$$F_{xi} \cong T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left. \frac{\Delta V}{\Delta t} \right|_i + V_{xi} \left. \frac{\Delta m}{\Delta t} \right|_i$$

1st Order Backwards Difference

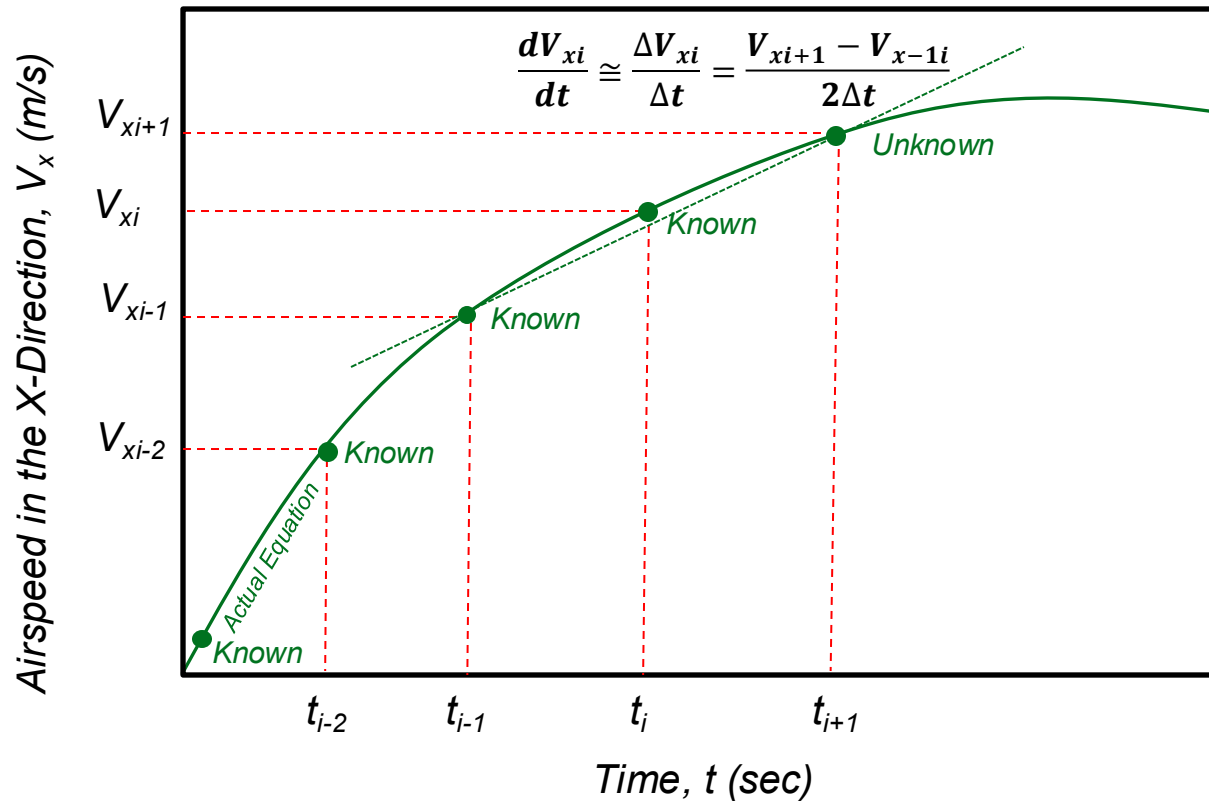


1st Order Proverse Engineering

Primer on Finite Difference Techniques & Numerical Solution

$$F_{xi} \cong T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left. \frac{\Delta V}{\Delta t} \right|_i + V_{xi} \left. \frac{\Delta m}{\Delta t} \right|_i$$

1st Order Centered Difference



1st Order Proverse Engineering

Primer on Finite Difference Techniques & Numerical Solution

Higher Order Accuracy:

$$\begin{aligned}
 & \left. \begin{aligned}
 f(x_{i+1}) &= f(x_i) + \Delta x f'(x_i) + \frac{\Delta x^2}{2!} f''(x_i) + O(\Delta x^3) \\
 f(x_{i+2}) &= f(x_i) + 2\Delta x f'(x_i) + \frac{4\Delta x^2}{2!} f''(x_i) + O(\Delta x^3)
 \end{aligned} \right\} \begin{array}{l} *(-2) \\ *(1) \end{array} \Rightarrow f''(x_i) = \frac{f(x_{i+2}) - 2f(x_{i+1}) + f(x_i)}{\Delta x^2} + O(\Delta x)
 \end{aligned}$$

$$f'(x_i) = \frac{f(x_{i+1}) - f(x_i)}{\Delta x} - \frac{\Delta x}{2!} f''(x_i) + O(\Delta x^2)$$

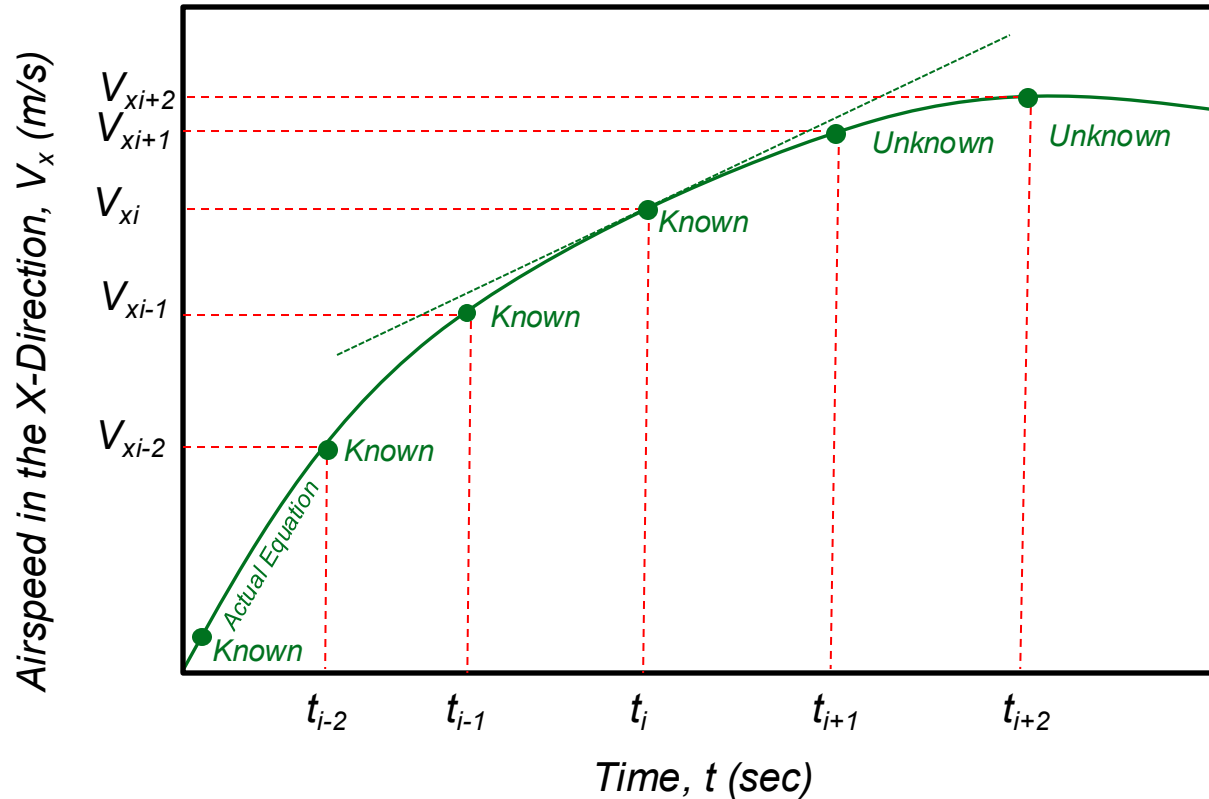
$$\Rightarrow \underline{f'(x_i)} = \underline{\frac{f(x_{i+1}) - f(x_i)}{\Delta x} - \frac{\Delta x}{2!} \frac{f(x_{i+2}) - 2f(x_{i+1}) + f(x_i)}{\Delta x^2} + O(\Delta x^2)} = \underline{\underline{\frac{-f(x_{i+2}) + 4f(x_{i+1}) - 3f(x_i)}{2\Delta x} + O(\Delta x^2)}}}$$

1st Order Proverse Engineering

Primer on Finite Difference Techniques & Numerical Solution

$$F_{xi} \cong T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left. \frac{\Delta V}{\Delta t} \right|_i + V_{xi} \left. \frac{\Delta m}{\Delta t} \right|_i$$

2nd Order Forward Difference $\frac{dV_{xi}}{dt} \cong \frac{\Delta V_{xi}}{\Delta t} = \frac{-V_{xi+2} + 4V_{xi+1} - 3V_{xi}}{2\Delta t}$



1st Order Proverse Engineering

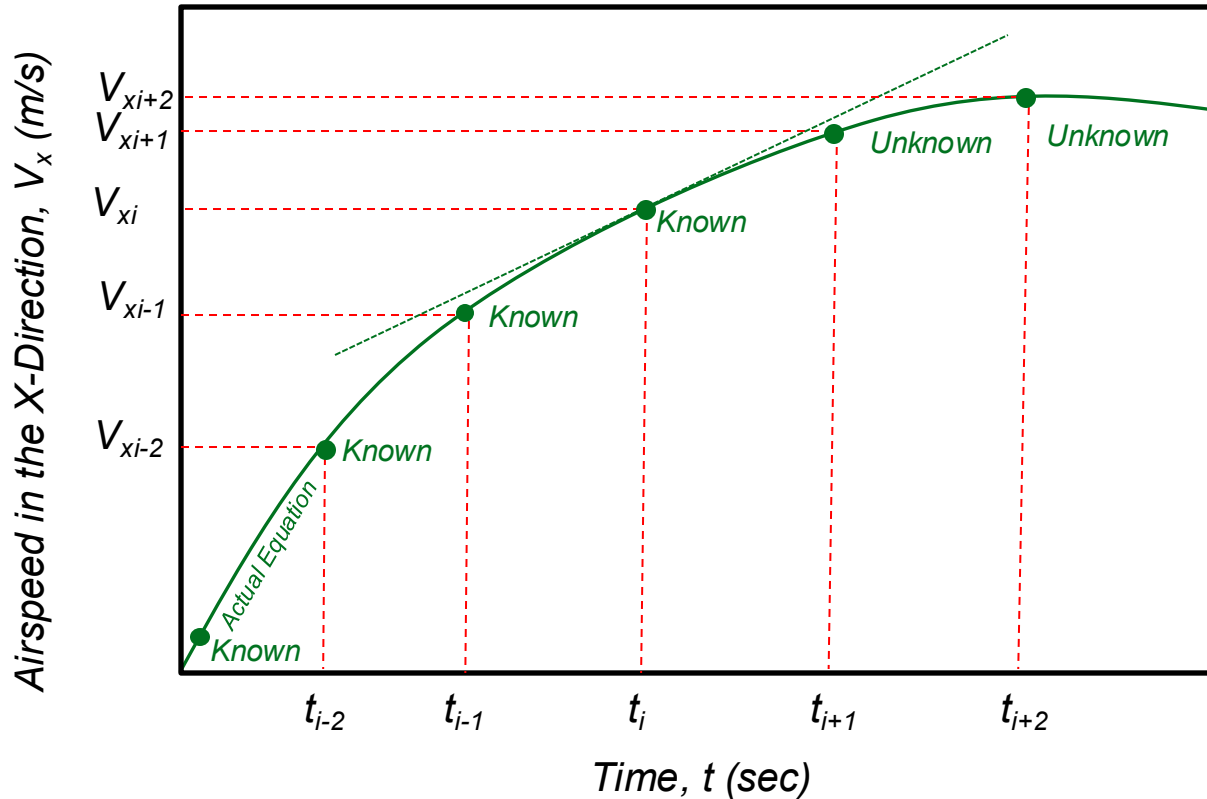
Primer on Finite Difference Techniques & Numerical Solution

$$F_{xi} \cong T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left. \frac{\Delta V}{\Delta t} \right|_i + V_{xi} \left. \frac{\Delta m}{\Delta t} \right|_i$$

Decremental

2nd Order Forward Difference

$$\frac{dV_{xi}}{dt} \cong \frac{\Delta V_{xi}}{\Delta t} = \frac{-V_{xi+1} + 4V_{xi} - 3V_{xi-1}}{2\Delta t}$$



1st Order Proverse Engineering

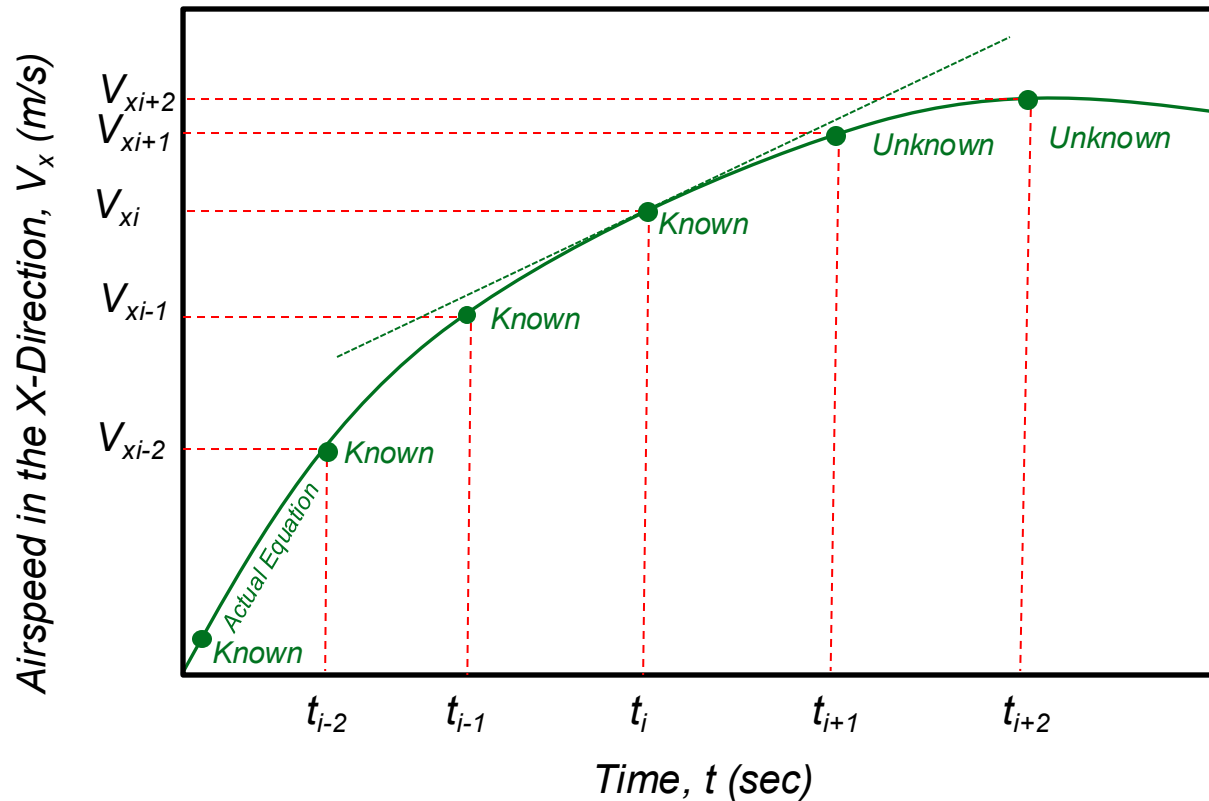
Primer on Finite Difference Techniques & Numerical Solution

$$F_{xi} \cong T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left. \frac{\Delta V}{\Delta t} \right|_i + V_{xi} \left. \frac{\Delta m}{\Delta t} \right|_i$$

Padé Approximation

4th Order Center Difference

$$\frac{dV_{xi}}{dt} \cong \frac{\Delta V_{xi}}{\Delta t} = \frac{-V_{xi+2} + 8V_{xi+1} - 8V_{xi-1} + V_{xi-2}}{12\Delta t}$$



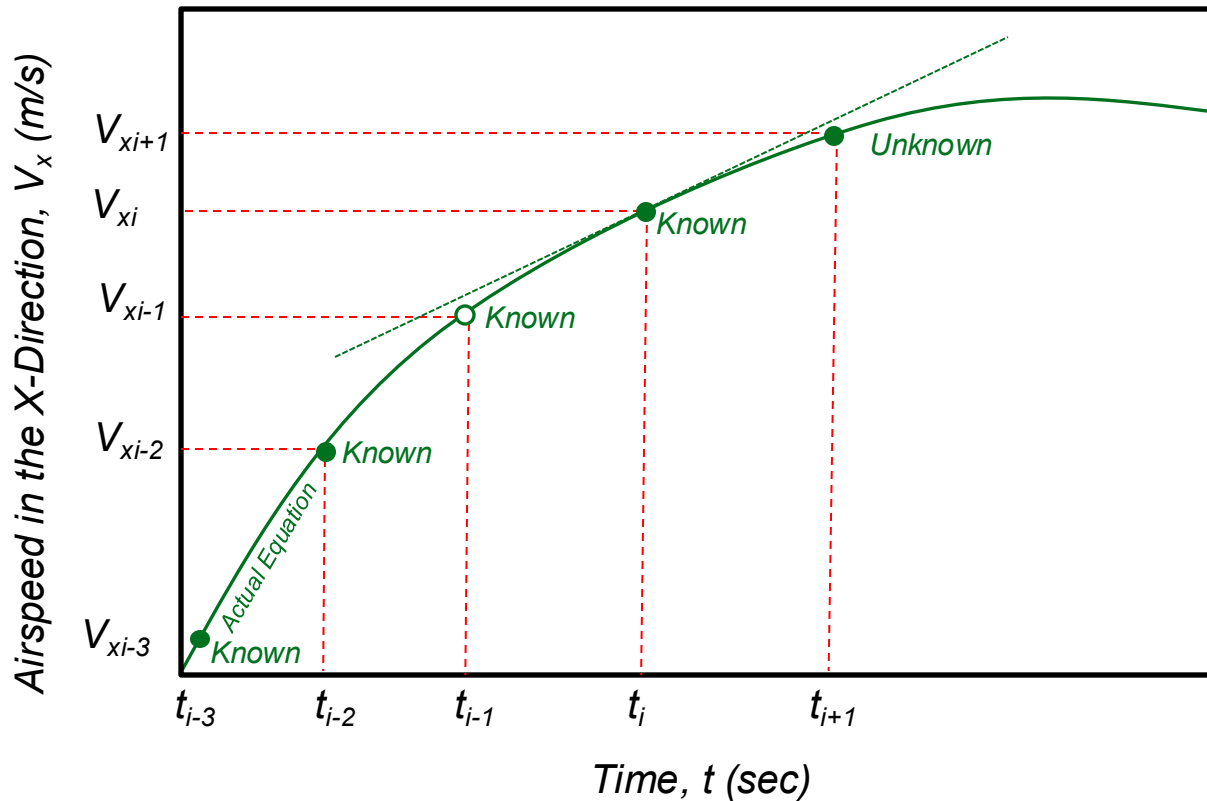
1st Order Proverse Engineering

Primer on Finite Difference Techniques & Numerical Solution

$$F_{xi} \cong T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left. \frac{\Delta V}{\Delta t} \right|_i + V_{xi} \left. \frac{\Delta m}{\Delta t} \right|_i$$

Padé Approximation Decremental
4th Order Forward Difference

$$\frac{dV_{xi}}{dt} \cong \frac{\Delta V_{xi}}{\Delta t} = \frac{-V_{xi+1} + 8V_{xi} - 8V_{xi-2} + V_{xi-3}}{12\Delta t}$$



1st Order Proverse Engineering

Primer on Finite Difference Techniques & Numerical Solution

$$T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left(\frac{-V_{xi+1} + 8V_{xi} - 8V_{xi-2} + V_{xi-3}}{12\Delta t} \right) + V_{xi} \left. \frac{\Delta m}{\Delta t} \right|_i$$

$$T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left(\frac{-V_{xi+1} + 8V_{xi} - 8V_{xi-2} + V_{xi-3}}{12\Delta t} \right) + V_{xi} \left. \frac{\Delta m}{\Delta t} \right|_i$$

Recall: I_{sp}

$$I_{sp} = \frac{T}{\dot{W}_f} = \frac{T}{g\dot{m}_f} = \frac{T}{g \frac{dm_f}{dt}} \cong \frac{T}{g \frac{\Delta m_f}{\Delta t}} \quad \therefore \quad \left. \frac{\Delta m}{\Delta t} \right|_i = \frac{T}{\dot{W}_f} = \frac{T}{g\dot{m}_f} = \frac{T}{g \frac{dm_f}{dt}} \cong \frac{T_i}{g I_{spi}}$$

1st Order Proverse Engineering

Primer on Finite Difference Techniques & Numerical Solution

$$T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left(\frac{-V_{xi+1} + 8V_{xi} - 8V_{xi-2} + V_{xi-3}}{12\Delta t} \right) + V_{xi} \left. \frac{\Delta m}{\Delta t} \right|_i$$

$$T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left(\frac{-V_{xi+1} + 8V_{xi} - 8V_{xi-2} + V_{xi-3}}{12\Delta t} \right) + V_{xi} \left. \frac{\Delta m}{\Delta t} \right|_i$$

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$$T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left(\frac{-V_{xi+1} + 8V_{xi} - 8V_{xi-2} + V_{xi-3}}{12\Delta t} \right) + V_{xi} \frac{T_i}{g I_{spi}}$$

1st Order Proverse Engineering

Primer on Finite Difference Techniques & Numerical Solution

$$T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left(\frac{-V_{xi+1} + 8V_{xi} - 8V_{xi-2} + V_{xi-3}}{12\Delta t} \right) + V_{xi} \left. \frac{\Delta m}{\Delta t} \right|_i$$

$$T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left(\frac{-V_{xi+1} + 8V_{xi} - 8V_{xi-2} + V_{xi-3}}{12\Delta t} \right) + V_{xi} \left. \frac{\Delta m}{\Delta t} \right|_i$$

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$$T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) - C_{Di} q_i A \cos \gamma_i - C_L q A \sin \gamma_i \cong m_i \left(\frac{-V_{xi+1} + 8V_{xi} - 8V_{xi-2} + V_{xi-3}}{12\Delta t} \right) + V_{xi} \frac{T_i}{g I_{spi}}$$

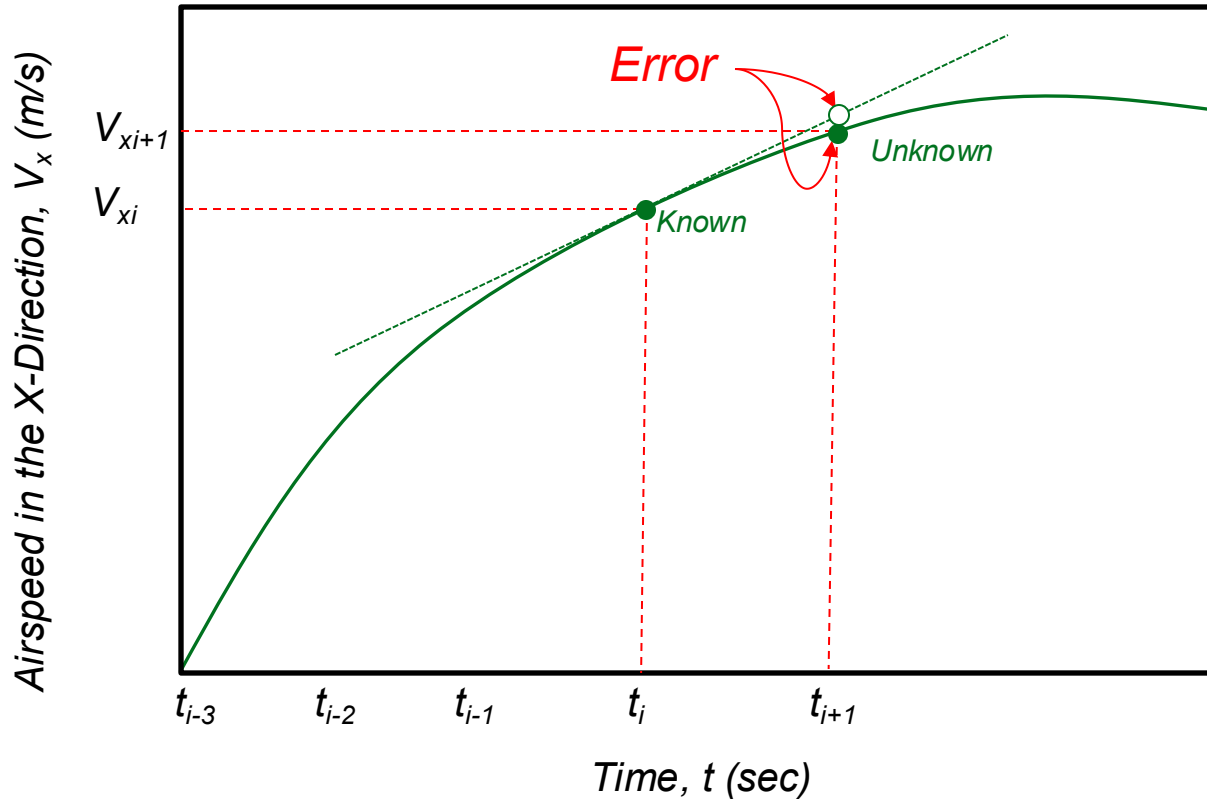
$$V_{xi+1} = \frac{12\Delta t}{m_i} \left[C_{Di} q_i A \cos \gamma_i + C_L q A \sin \gamma_i - T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) + V_{xi} \frac{T_i}{g I_{spi}} \right] + 8V_{xi} - 8V_{xi-2} + V_{xi-3}$$

1st Order Proverse Engineering

1st Order approximations for V_{i+1}

$$\frac{dV_{xi}}{dt} \cong \frac{\Delta V_{xi}}{\Delta t} = \frac{V_{xi+1} - V_{xi}}{\Delta t} \quad \therefore \quad V_{xi+1} = \left. \frac{dV_x}{dt} \right|_i \Delta t + V_{xi}$$

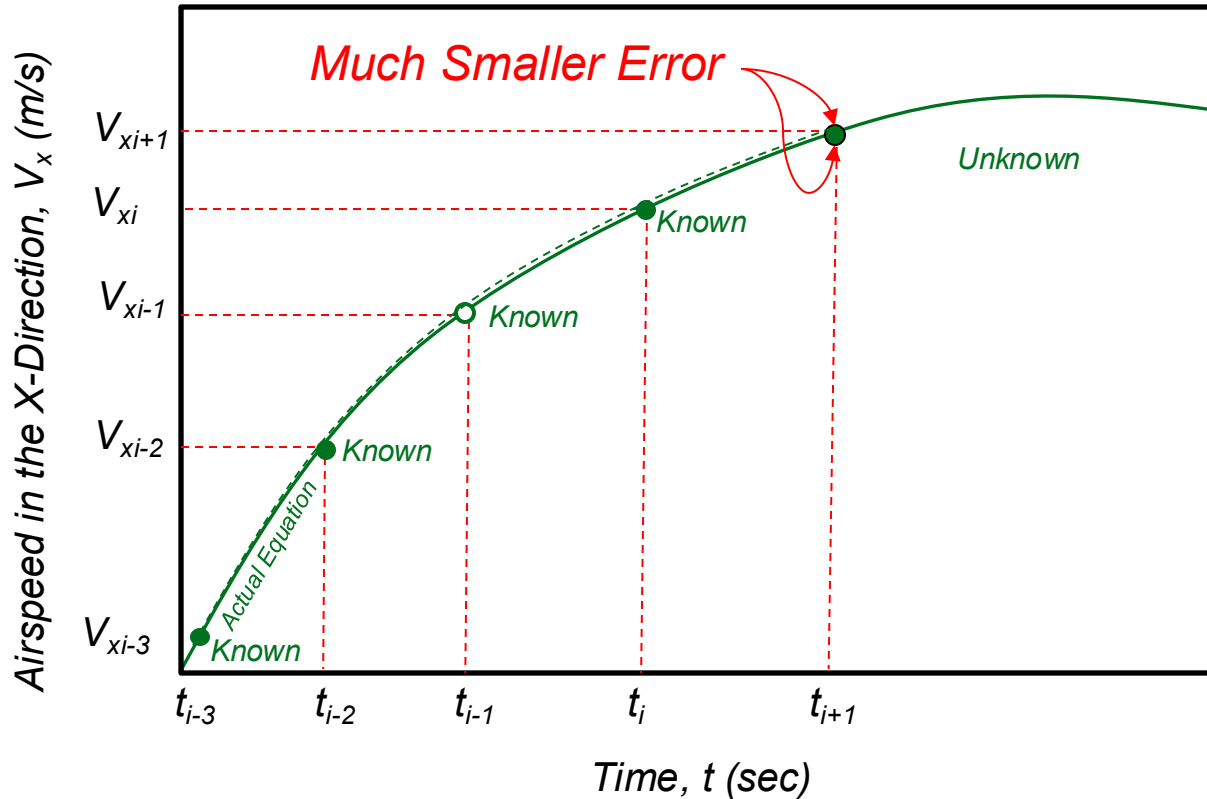
Error between estimate and exact expression



1st Order Proverse Engineering

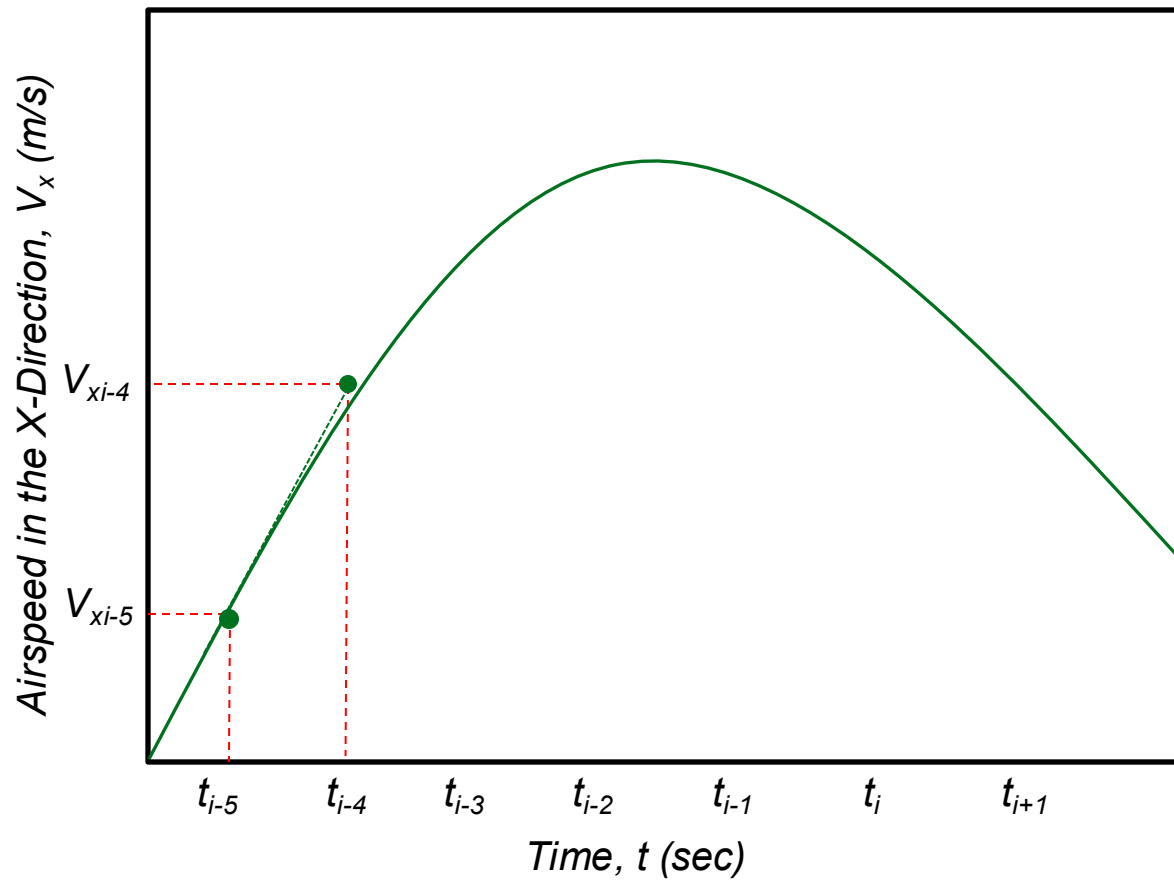
4th Order (Padé) approximations for V_{i+1}

$$\frac{dV_{xi}}{dt} \cong \frac{\Delta V_{xi}}{\Delta t} = \frac{-V_{xi+2} + 8V_{xi+1} - 8V_{xi-1} + V_{xi-2}}{12\Delta t} \quad \therefore \quad V_{xi+1} = +8V_{xi} - 8V_{xi-2} + V_{xi-3} - 12\Delta t \left. \frac{dV_x}{dt} \right|_i$$



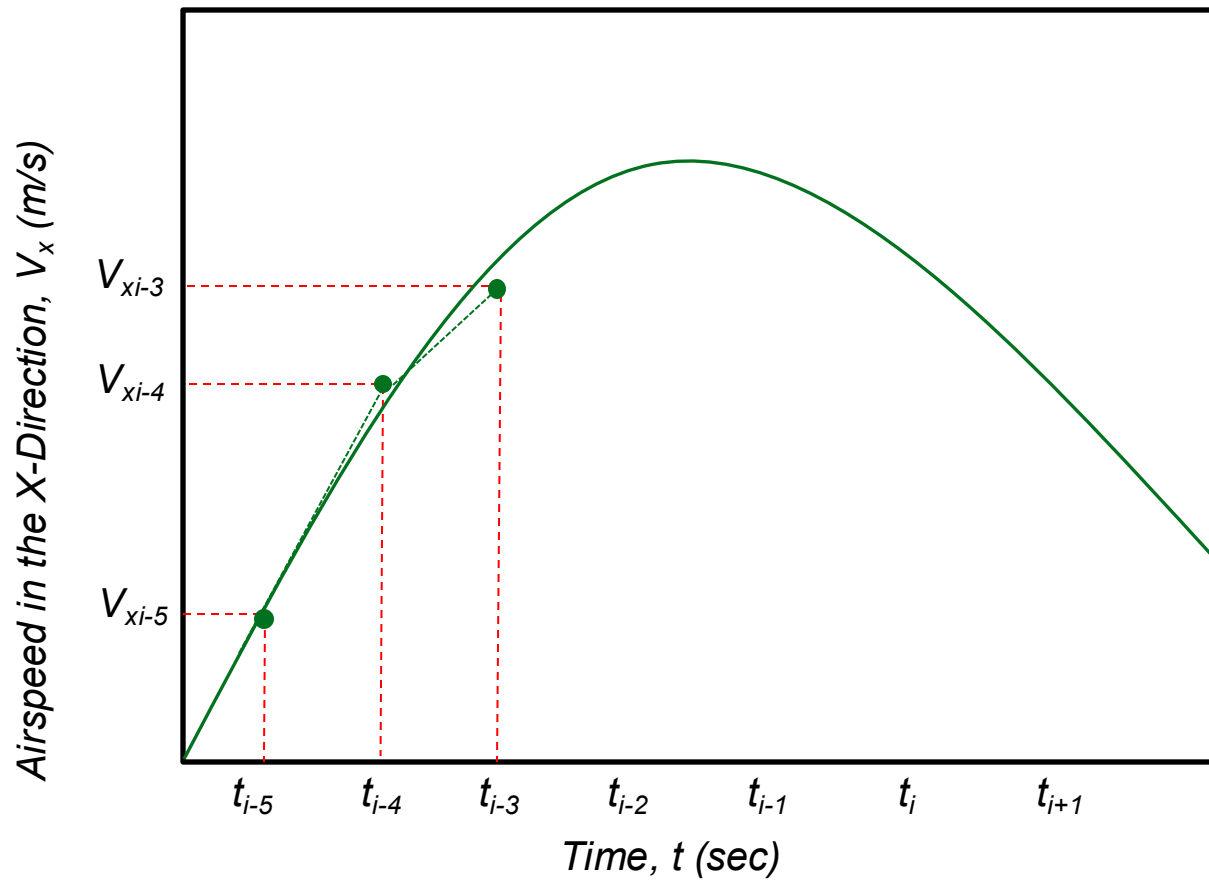
1st Order Proverse Engineering

Problems with Numerical Modeling



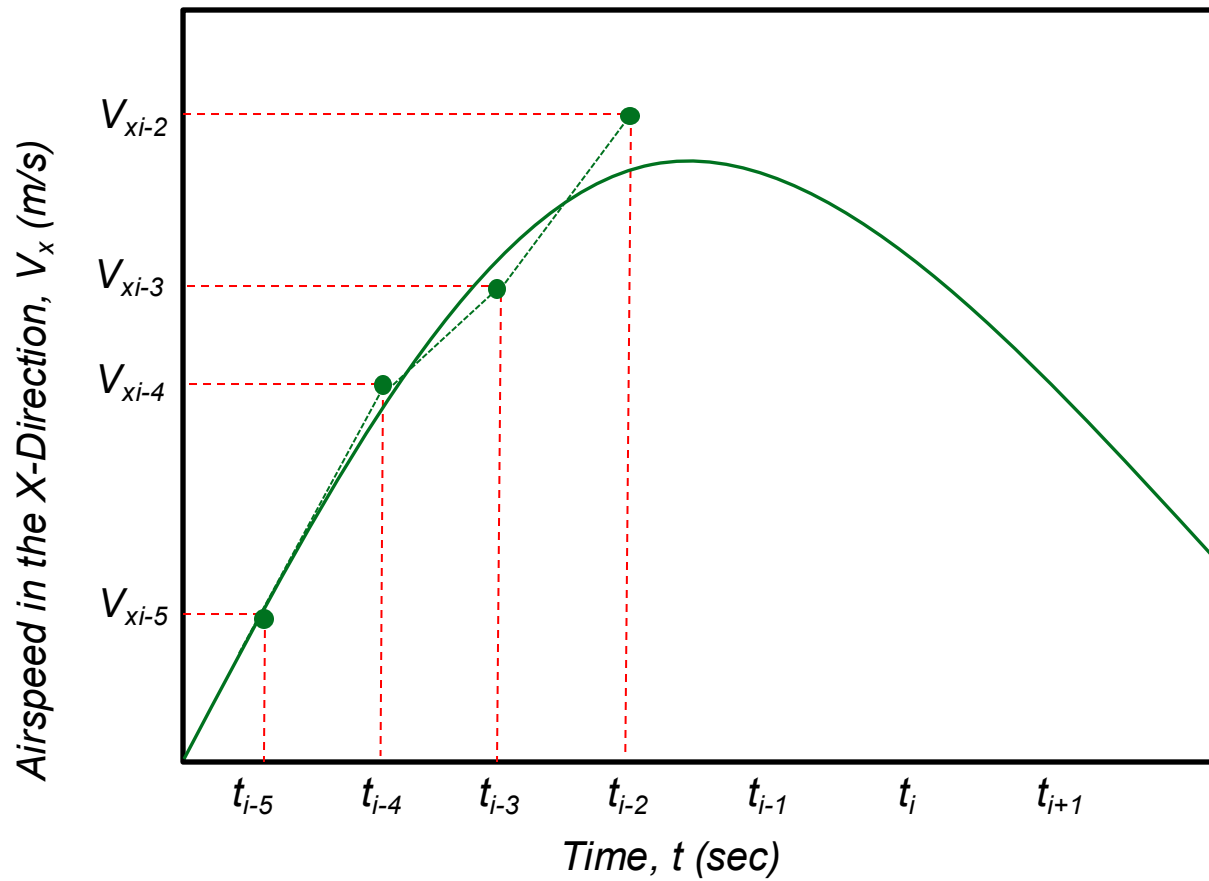
1st Order Proverse Engineering

Problems with Numerical Modeling



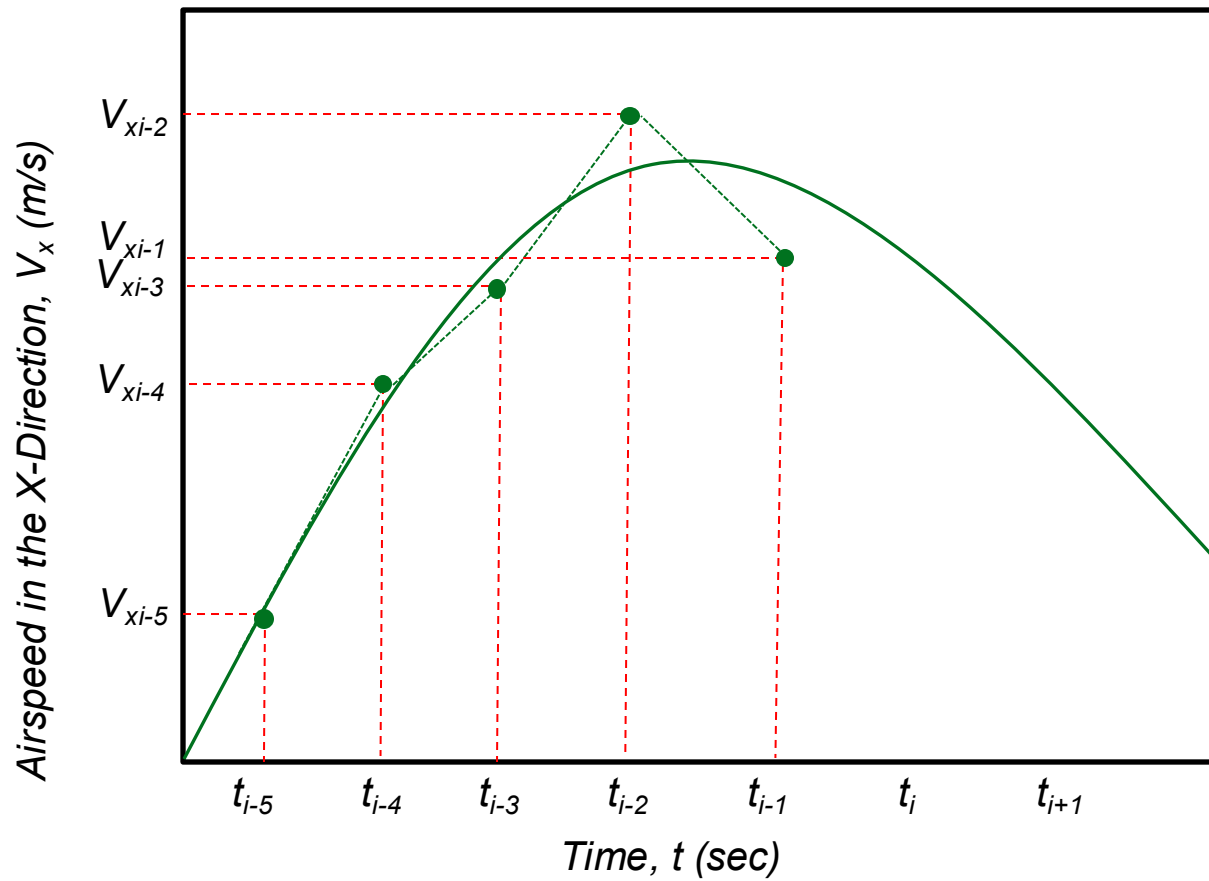
1st Order Proverse Engineering

Problems with Numerical Modeling



1st Order Proverse Engineering

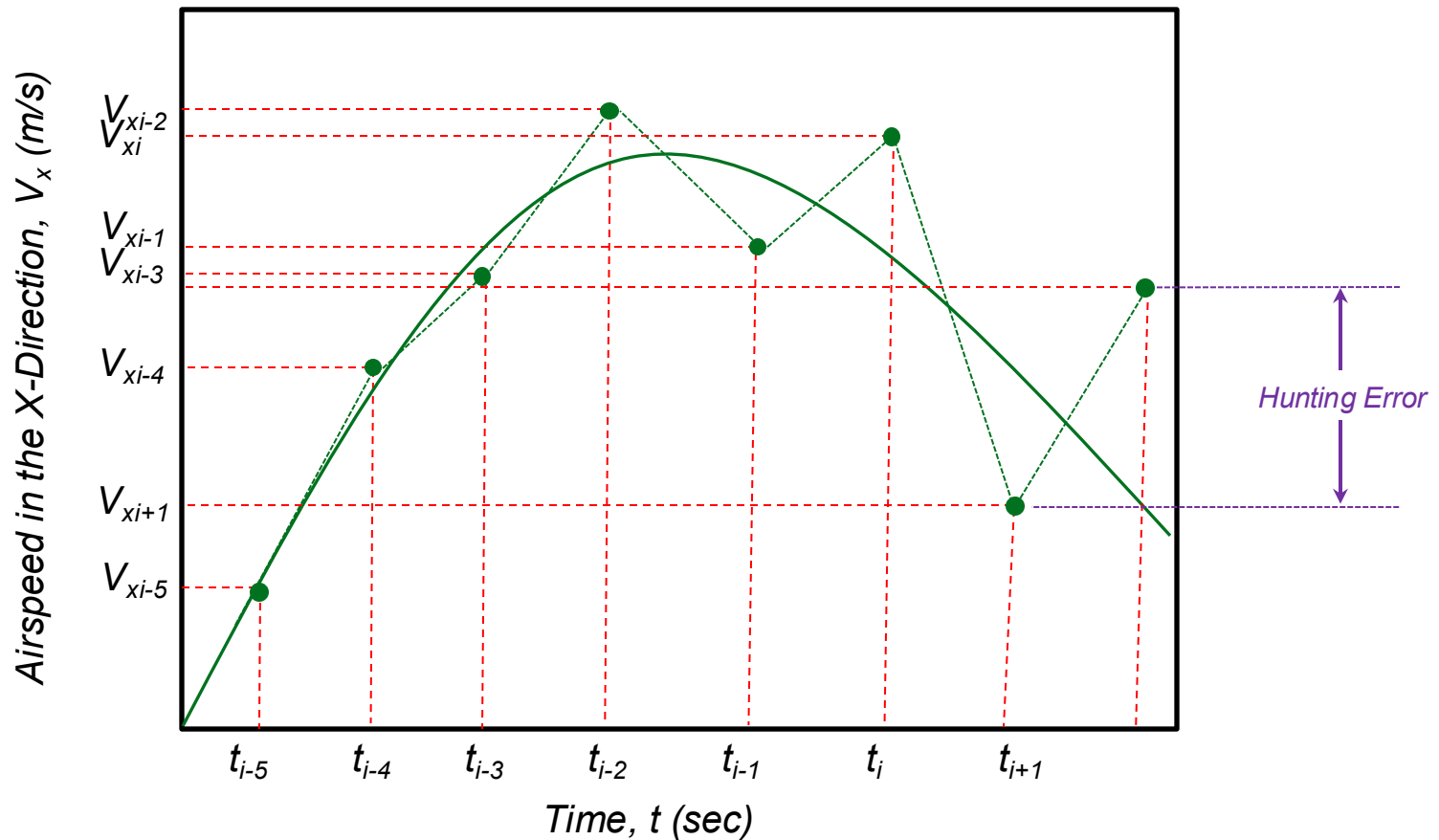
Problems with Numerical Modeling



1st Order Proverse Engineering

Problems with Numerical Modeling

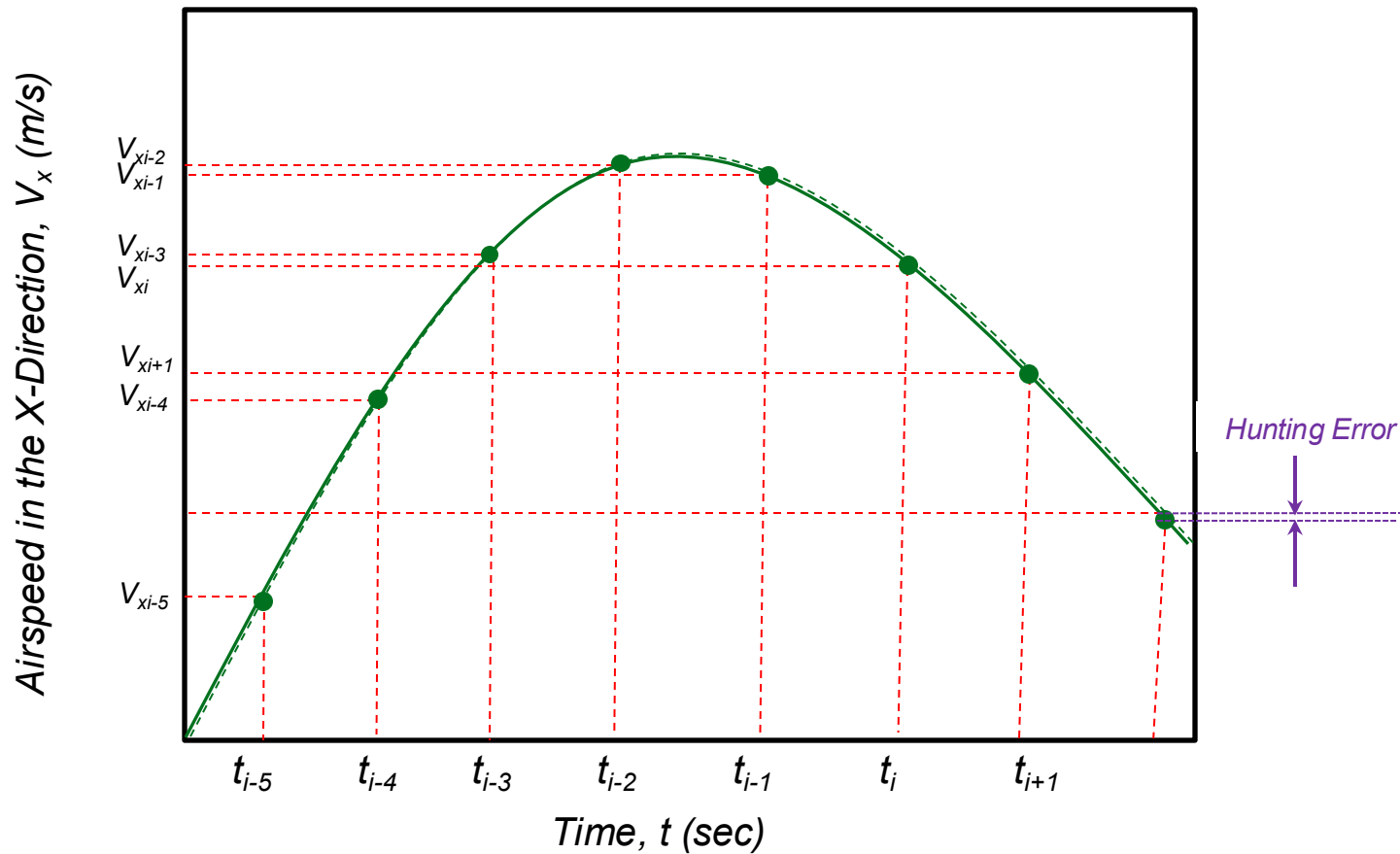
Numerical Instability: Steps too coarse for given function, order of estimation too low



1st Order Proverse Engineering

High Order Estimates

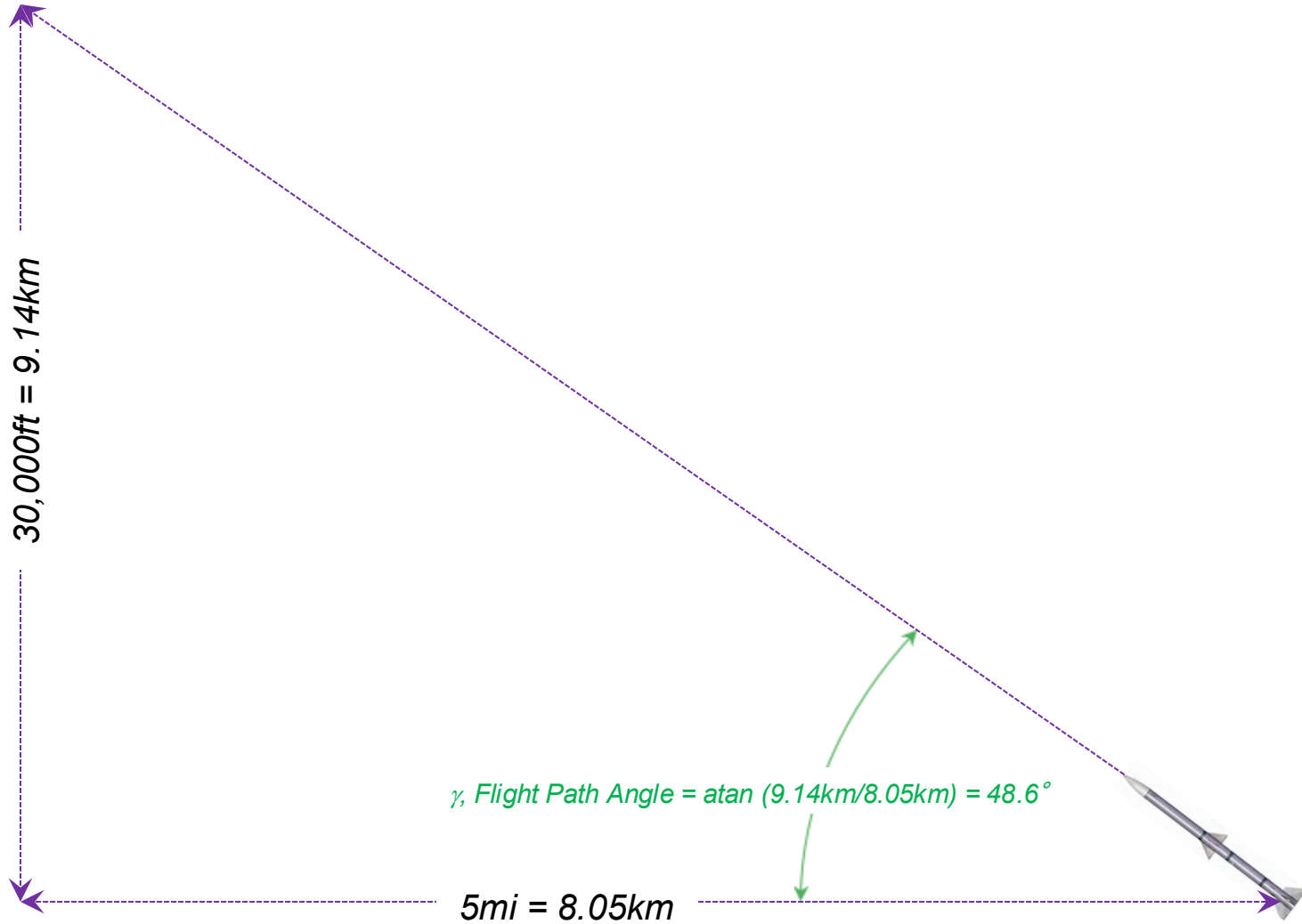
High order estimates allow coarser time steps with lower errors (faster codes)



1st Order Proverse Engineering

Coding the shot...

30,000 ft altitude @ 5 miles



1st Order Proverse Engineering

Coding the shot...

γ_i appears multiple times in eq. 5 & 6... and is extremely important

$$V_{xi+1} = \frac{12\Delta t}{m_i} \left[C_{Di} q_i A C \cos \gamma_i + C_{Li} q A S \sin \gamma_i - T_i \cos(\alpha_i + \phi_{ti} + \gamma_i) + V_{xi} \frac{T_i}{g I_{spi}} \right] + 8V_{xi} - 8V_{xi-2} + V_{xi-3}$$

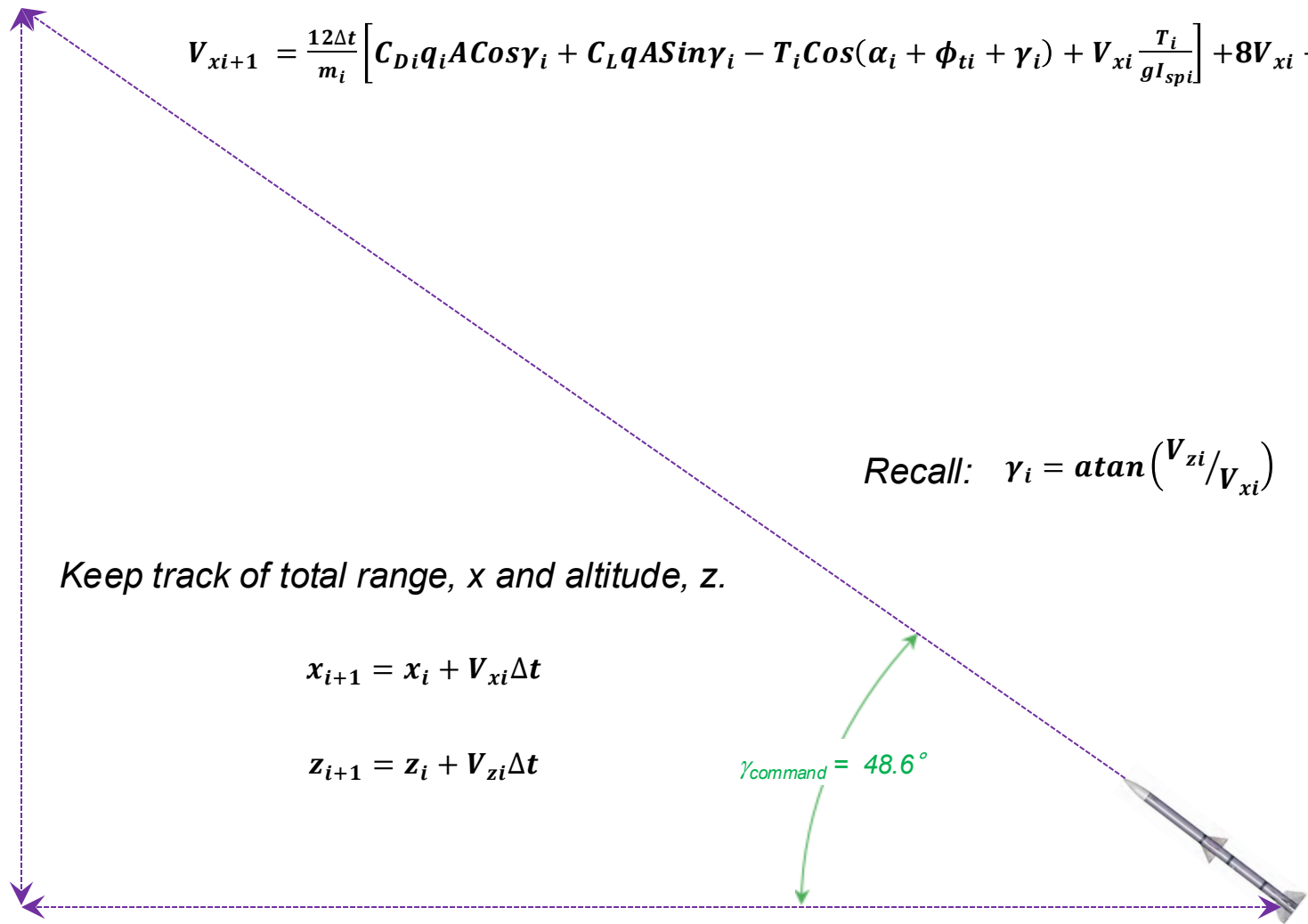
Recall: $\gamma_i = \text{atan}(V_{zi}/V_{xi})$

Keep track of total range, x and altitude, z .

$$x_{i+1} = x_i + V_{xi} \Delta t$$

$$z_{i+1} = z_i + V_{zi} \Delta t$$

$\gamma_{\text{command}} = 48.6^\circ$

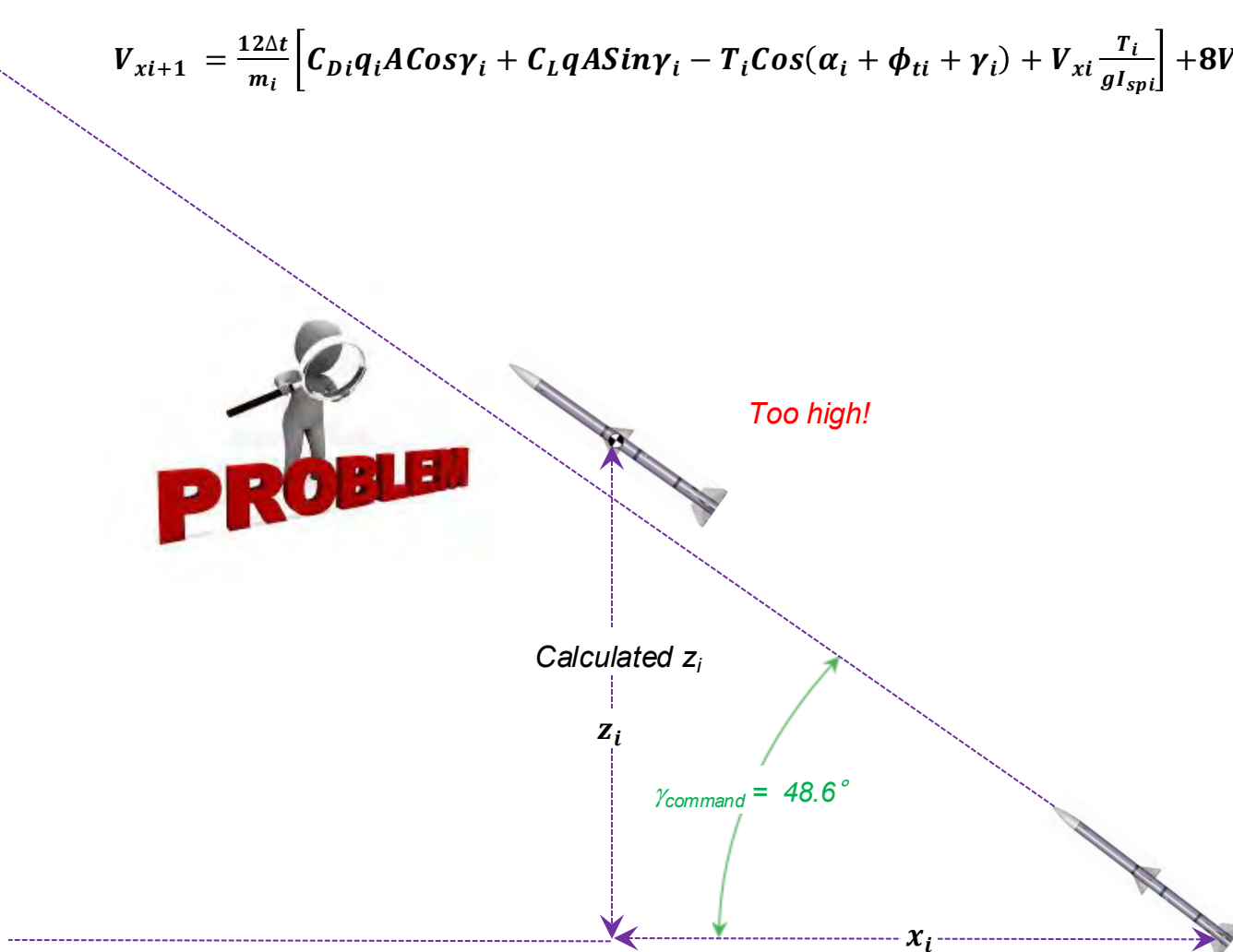


1st Order Proverse Engineering

Coding the shot...

Update the angle of attack to fly on trajectory:

$$V_{xi+1} = \frac{12\Delta t}{m_i} \left[C_{Di}q_iA\cos\gamma_i + C_LqAS\sin\gamma_i - T_i\cos(\alpha_i + \phi_{ti} + \gamma_i) + V_{xi} \frac{T_i}{gI_{spi}} \right] + 8V_{xi} - 8V_{xi-2} + V_{xi-3}$$

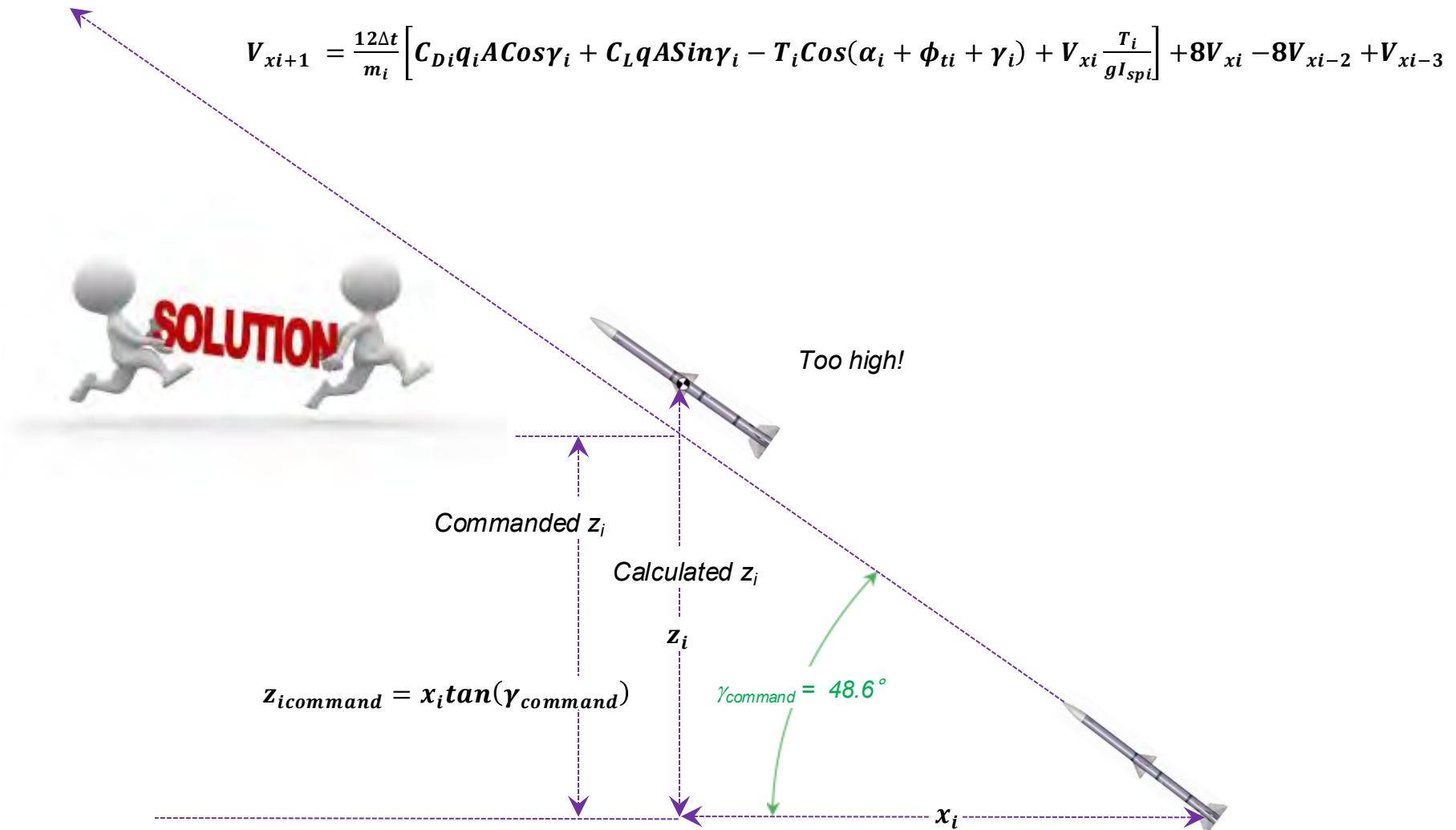


1st Order Proverse Engineering

Coding the shot...

Update the angle of attack to fly on trajectory:

$$V_{xi+1} = \frac{12\Delta t}{m_i} \left[C_{Di}q_iACos\gamma_i + C_LqASin\gamma_i - T_iCos(\alpha_i + \phi_{ti} + \gamma_i) + V_{xi} \frac{T_i}{gI_{spi}} \right] + 8V_{xi} - 8V_{xi-2} + V_{xi-3}$$



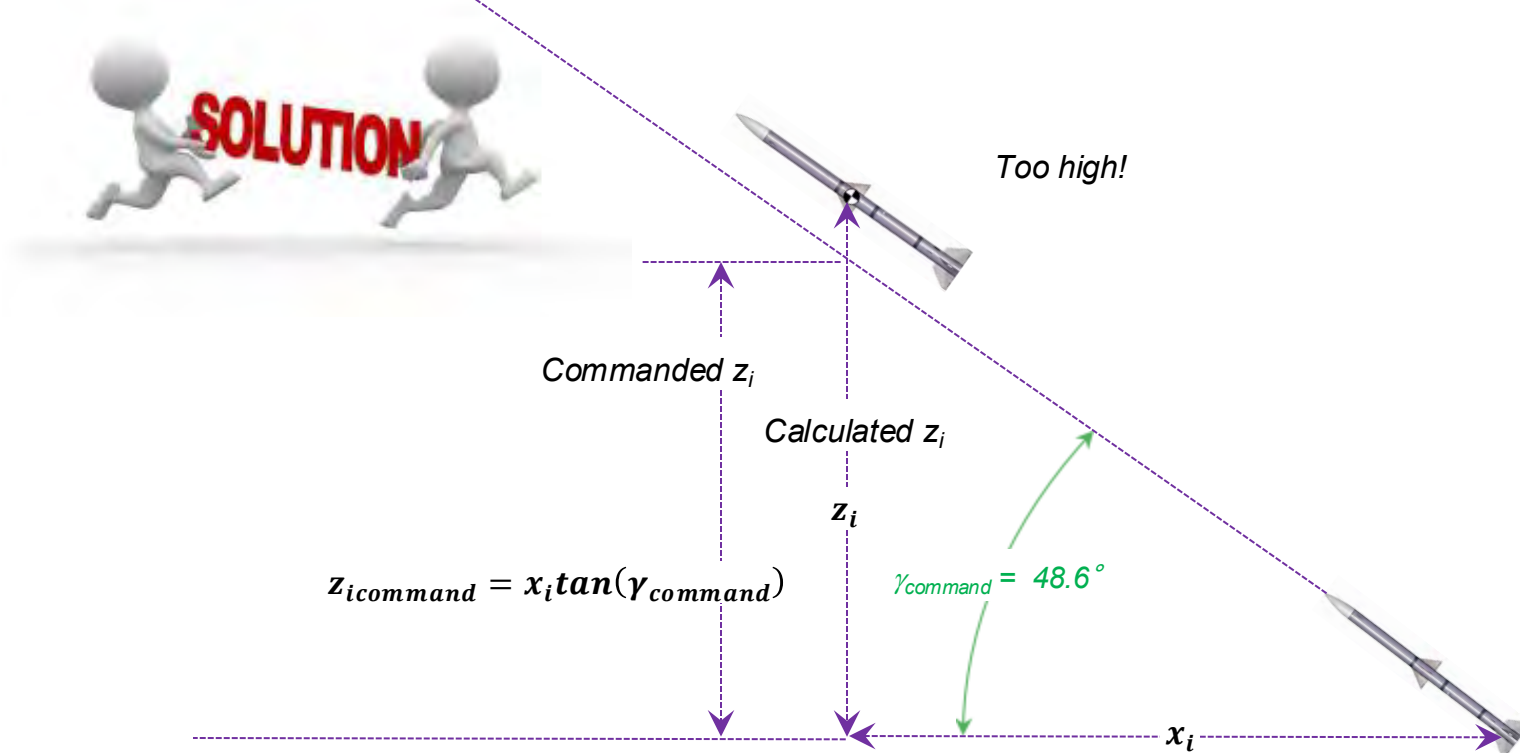
1st Order Proverse Engineering

Coding the shot...

Update the angle of attack to fly on trajectory:

$$V_{xi+1} = \frac{12\Delta t}{m_i} \left[C_{Di}q_iA\cos\gamma_i + C_LqAS\sin\gamma_i - T_i\cos(\alpha_i + \phi_{ti} + \gamma_i) + V_{xi} \frac{T_i}{gI_{spi}} \right] + 8V_{xi} - 8V_{xi-2} + V_{xi-3}$$

Cut altitude to intercept line by reducing α_{i+1}



1st Order Proverse Engineering

Coding the shot...

Update the angle of attack to fly on trajectory:

$$V_{xi+1} = \frac{12\Delta t}{m_i} \left[C_{Di}q_iA\cos\gamma_i + C_LqAS\sin\gamma_i - T_i\cos(\alpha_i + \phi_{ti} + \gamma_i) + V_{xi} \frac{T_i}{gI_{spi}} \right] + 8V_{xi} - 8V_{xi-2} + V_{xi-3}$$

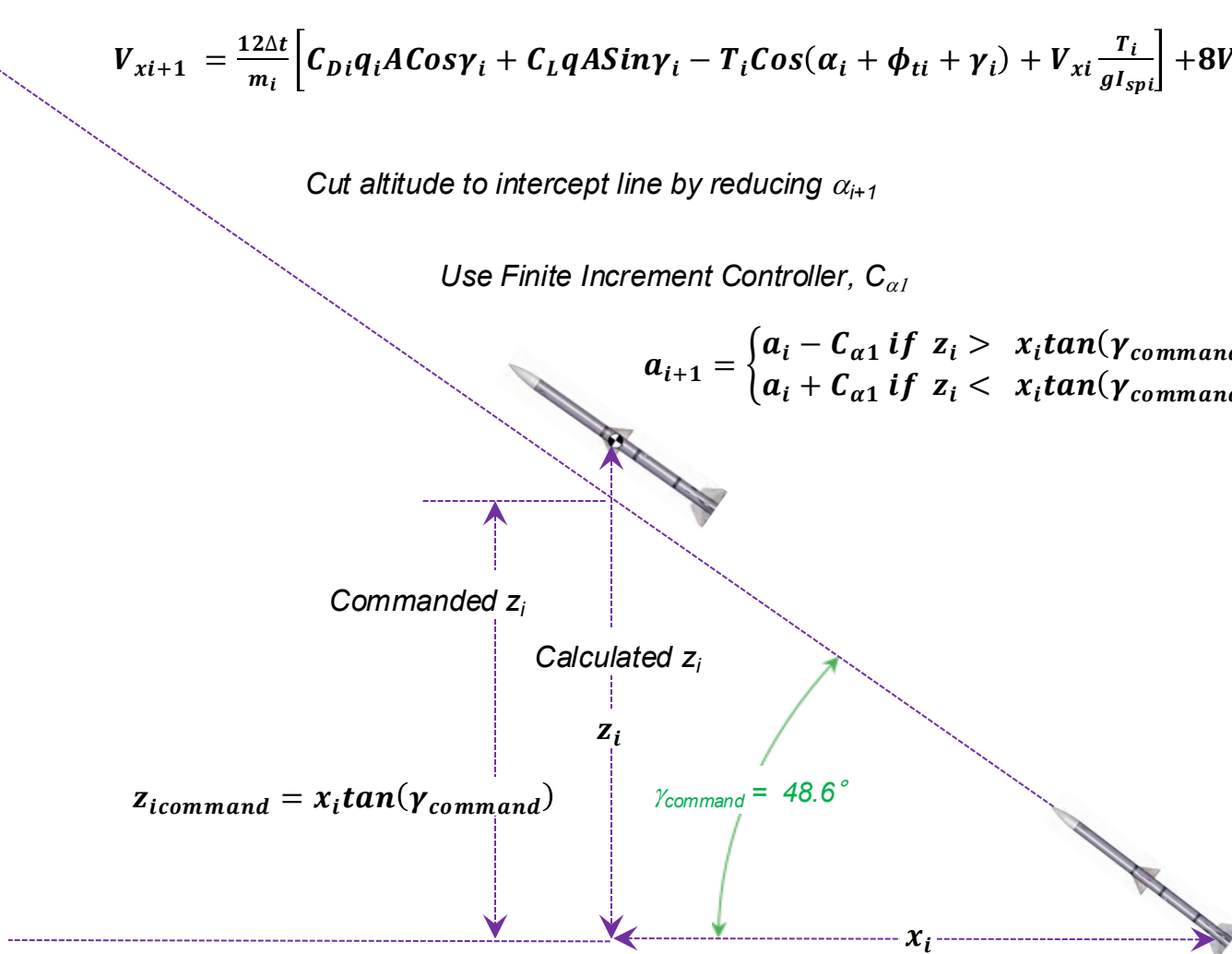
Cut altitude to intercept line by reducing α_{i+1}

Use Finite Increment Controller, $C_{\alpha 1}$

$$a_{i+1} = \begin{cases} a_i - C_{\alpha 1} & \text{if } z_i > x_i \tan(\gamma_{command}) \\ a_i + C_{\alpha 1} & \text{if } z_i < x_i \tan(\gamma_{command}) \end{cases}$$

$$z_{icommand} = x_i \tan(\gamma_{command})$$

$$\gamma_{command} = 48.6^\circ$$



1st Order Proverse Engineering

Coding the shot...

Update the angle of attack to fly on trajectory:

$$V_{xi+1} = \frac{12\Delta t}{m_i} \left[C_{Di}q_iA\cos\gamma_i + C_LqAS\sin\gamma_i - T_i\cos(\alpha_i + \phi_{ti} + \gamma_i) + V_{xi} \frac{T_i}{gI_{spi}} \right] + 8V_{xi} - 8V_{xi-2} + V_{xi-3}$$

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Where $C_{\alpha 1}$ is just a number, like 0.1 deg.

Commanded z_i

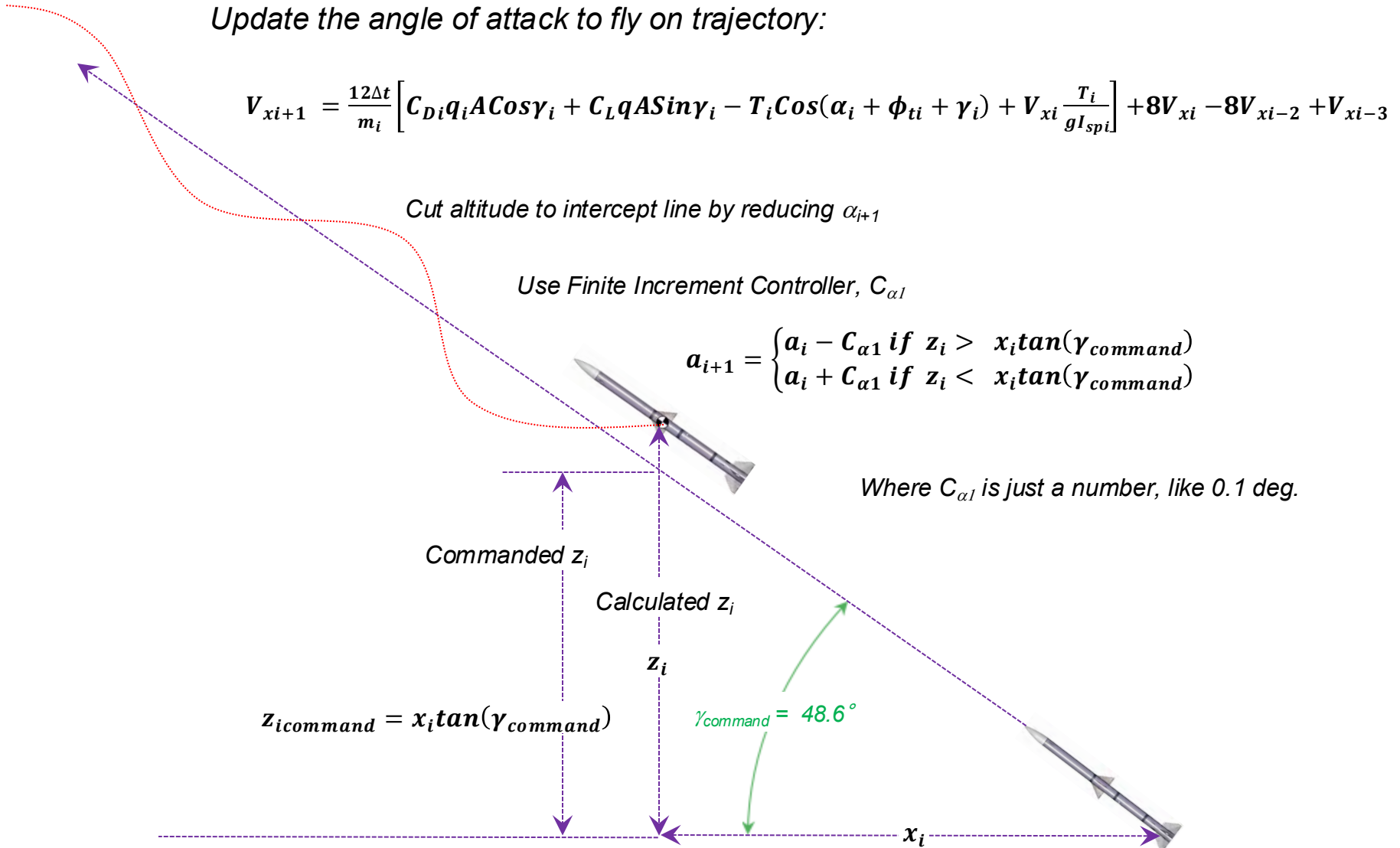
Calculated z_i

z_i

$$z_{icommand} = x_i \tan(\gamma_{command})$$

$$\gamma_{command} = 48.6^\circ$$

x_i



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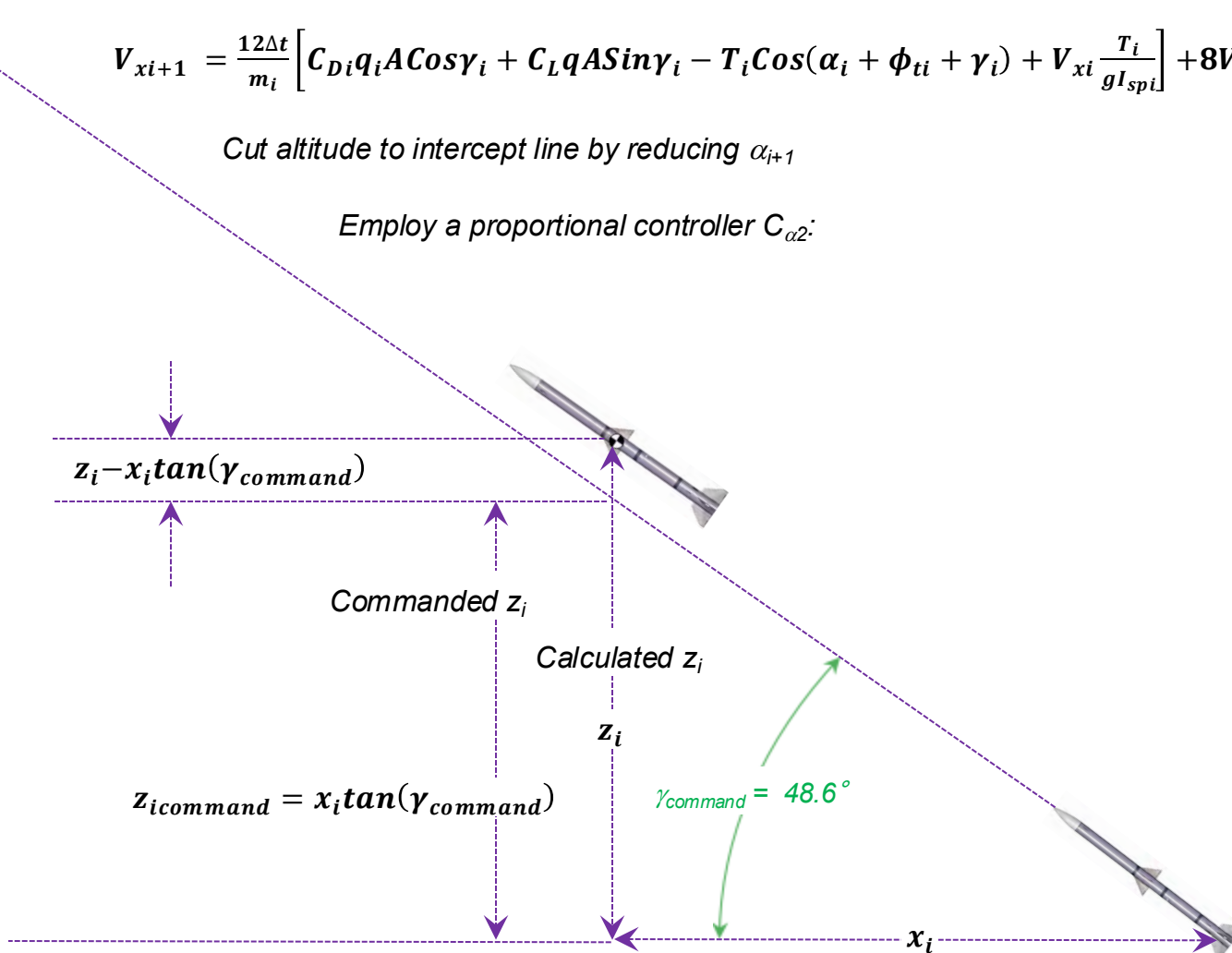
Coding the shot...

Update the angle of attack to fly on trajectory:

$$V_{xi+1} = \frac{12\Delta t}{m_i} \left[C_{Di}q_iA\cos\gamma_i + C_{L}qAS\sin\gamma_i - T_i\cos(\alpha_i + \phi_{ti} + \gamma_i) + V_{xi} \frac{T_i}{gI_{spi}} \right] + 8V_{xi} - 8V_{xi-2} + V_{xi-3}$$

Cut altitude to intercept line by reducing α_{i+1}

Employ a proportional controller $C_{\alpha 2}$:



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Coding the shot...

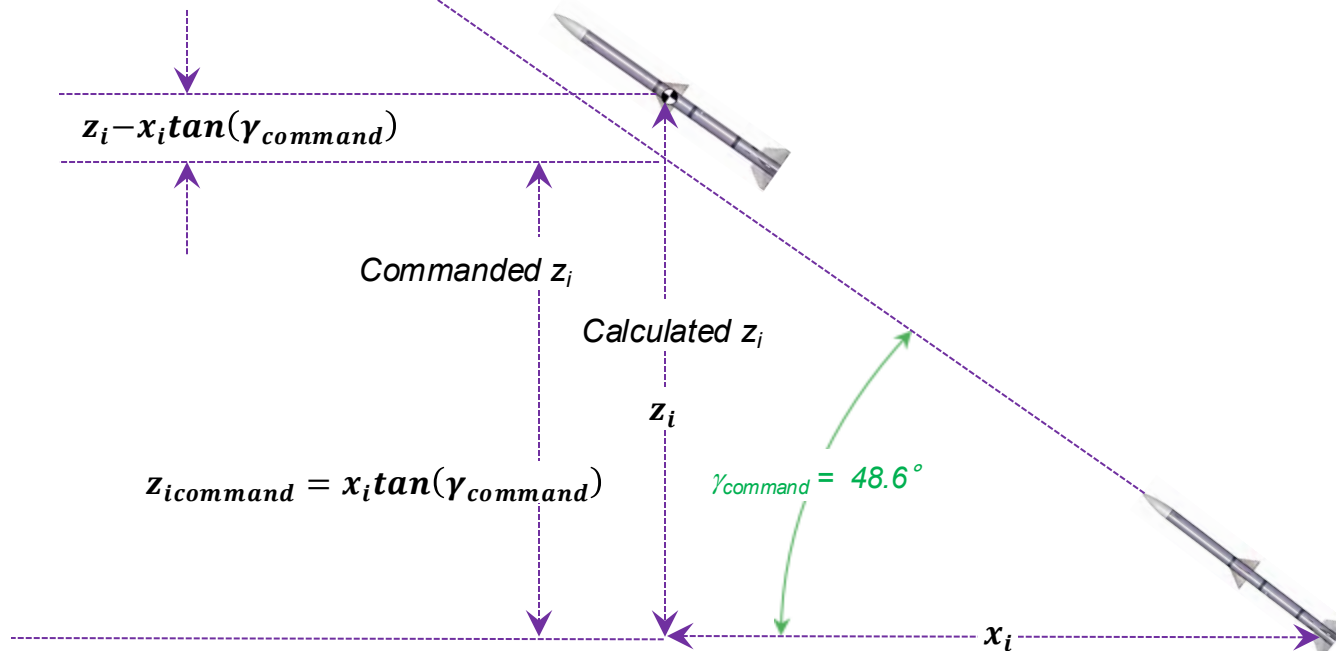
Update the angle of attack to fly on trajectory:

$$V_{xi+1} = \frac{12\Delta t}{m_i} \left[C_{Di}q_iA\cos\gamma_i + C_LqAS\sin\gamma_i - T_i\cos(\alpha_i + \phi_{ti} + \gamma_i) + V_{xi} \frac{T_i}{gI_{spi}} \right] + 8V_{xi} - 8V_{xi-2} + V_{xi-3}$$

Cut altitude to intercept line by reducing α_{i+1}

Employ a proportional controller $C_{\alpha 2}$:

$$a_{i+1} = \begin{cases} a_i - C_{\alpha 1} - C_{\alpha 2} [z_i - x_i \tan(\gamma_{command})] & \text{if } z_i > x_i \tan(\gamma_{command}) \\ a_i + C_{\alpha 1} + C_{\alpha 2} [z_i - x_i \tan(\gamma_{command})] & \text{if } z_i < x_i \tan(\gamma_{command}) \end{cases}$$



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Coding the shot...

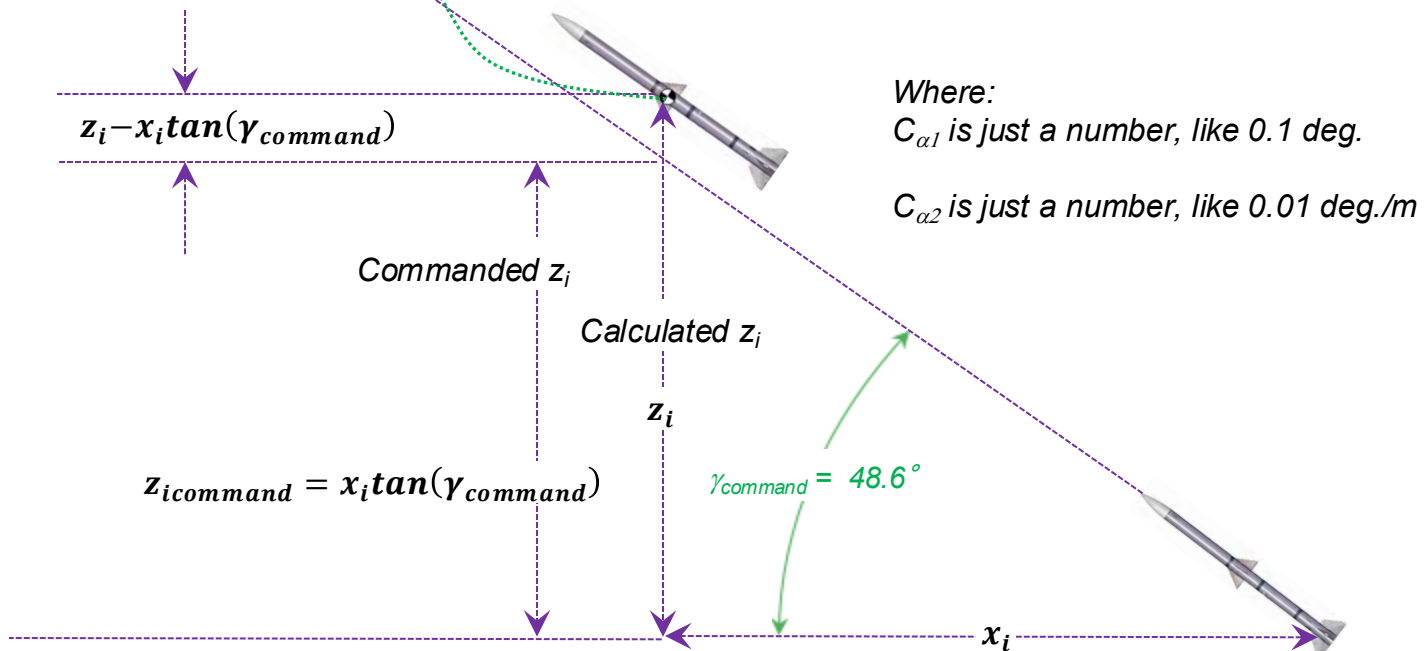
Update the angle of attack to fly on trajectory:

$$V_{xi+1} = \frac{12\Delta t}{m_i} \left[C_{Di}q_iA\cos\gamma_i + C_LqAS\sin\gamma_i - T_i\cos(\alpha_i + \phi_{ti} + \gamma_i) + V_{xi} \frac{T_i}{gI_{spi}} \right] + 8V_{xi} - 8V_{xi-2} + V_{xi-3}$$

Cut altitude to intercept line by reducing α_{i+1}

Employ a proportional controller $C_{\alpha 2}$:

$$\alpha_{i+1} = \begin{cases} \alpha_i - C_{\alpha 1} - C_{\alpha 2} [z_i - x_i \tan(\gamma_{command})] & \text{if } z_i > x_i \tan(\gamma_{command}) \\ \alpha_i + C_{\alpha 1} + C_{\alpha 2} [z_i - x_i \tan(\gamma_{command})] & \text{if } z_i < x_i \tan(\gamma_{command}) \end{cases}$$

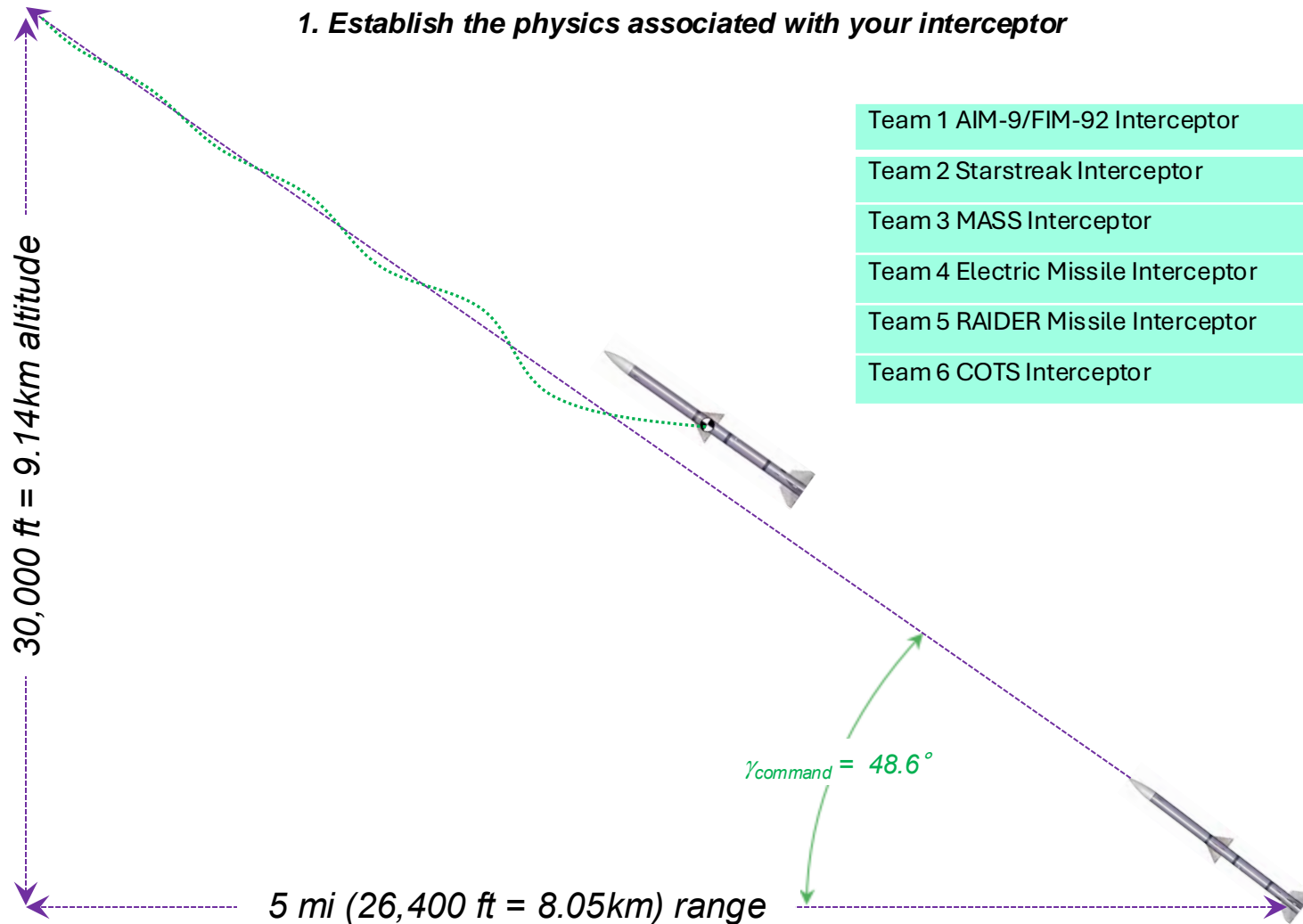


1st Order Proverse Engineering

Step back and examine the mission:

Proverse design a missile to make the shot

1. Establish the physics associated with your interceptor



Team 1 AIM-9/FIM-92 Interceptor

Team 2 Starstreak Interceptor

Team 3 MASS Interceptor

Team 4 Electric Missile Interceptor

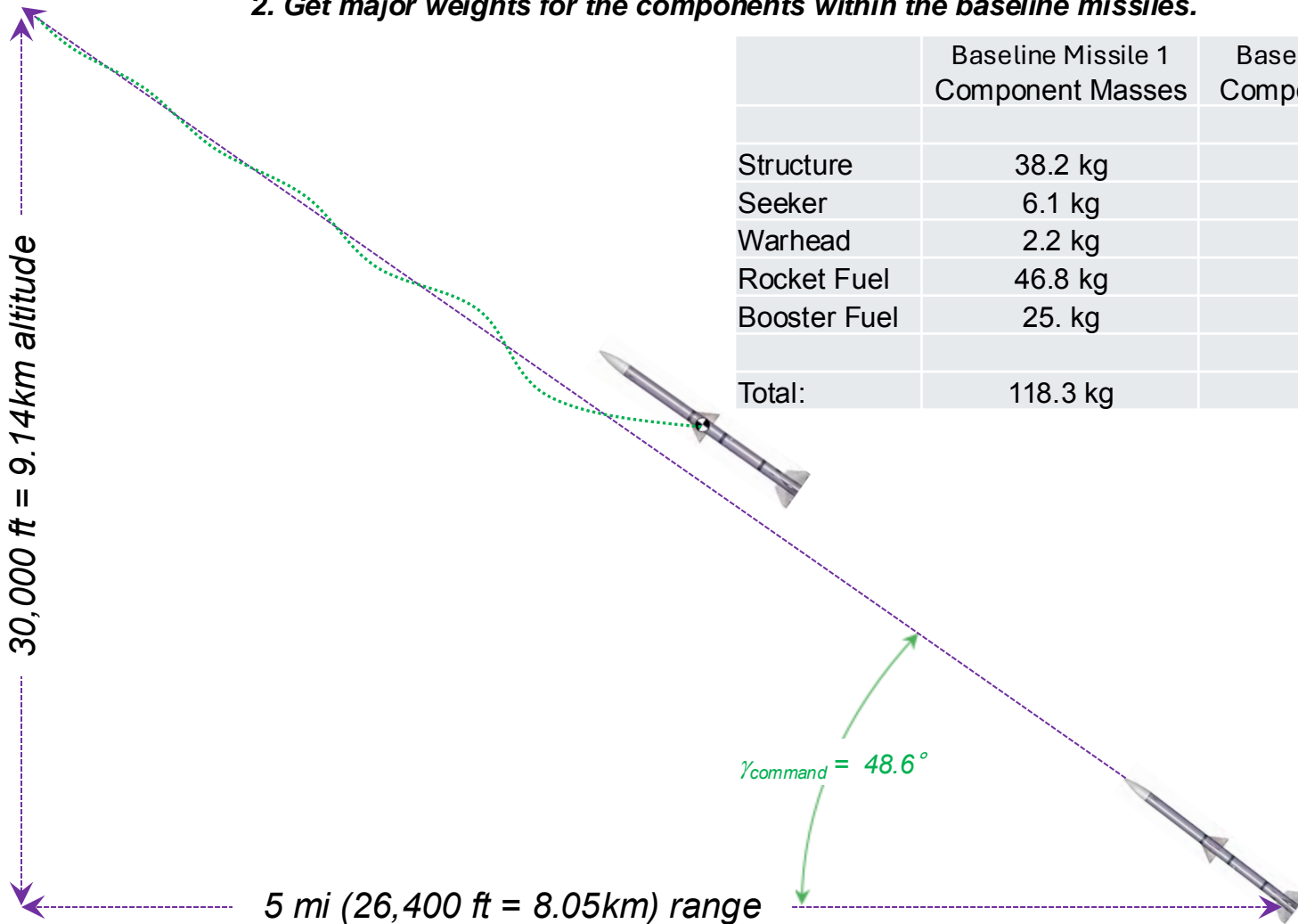
Team 5 RAIDER Missile Interceptor

Team 6 COTS Interceptor

1st Order Proverse Engineering

Proverse design a missile to make the shot

2. Get major weights for the components within the baseline missiles.



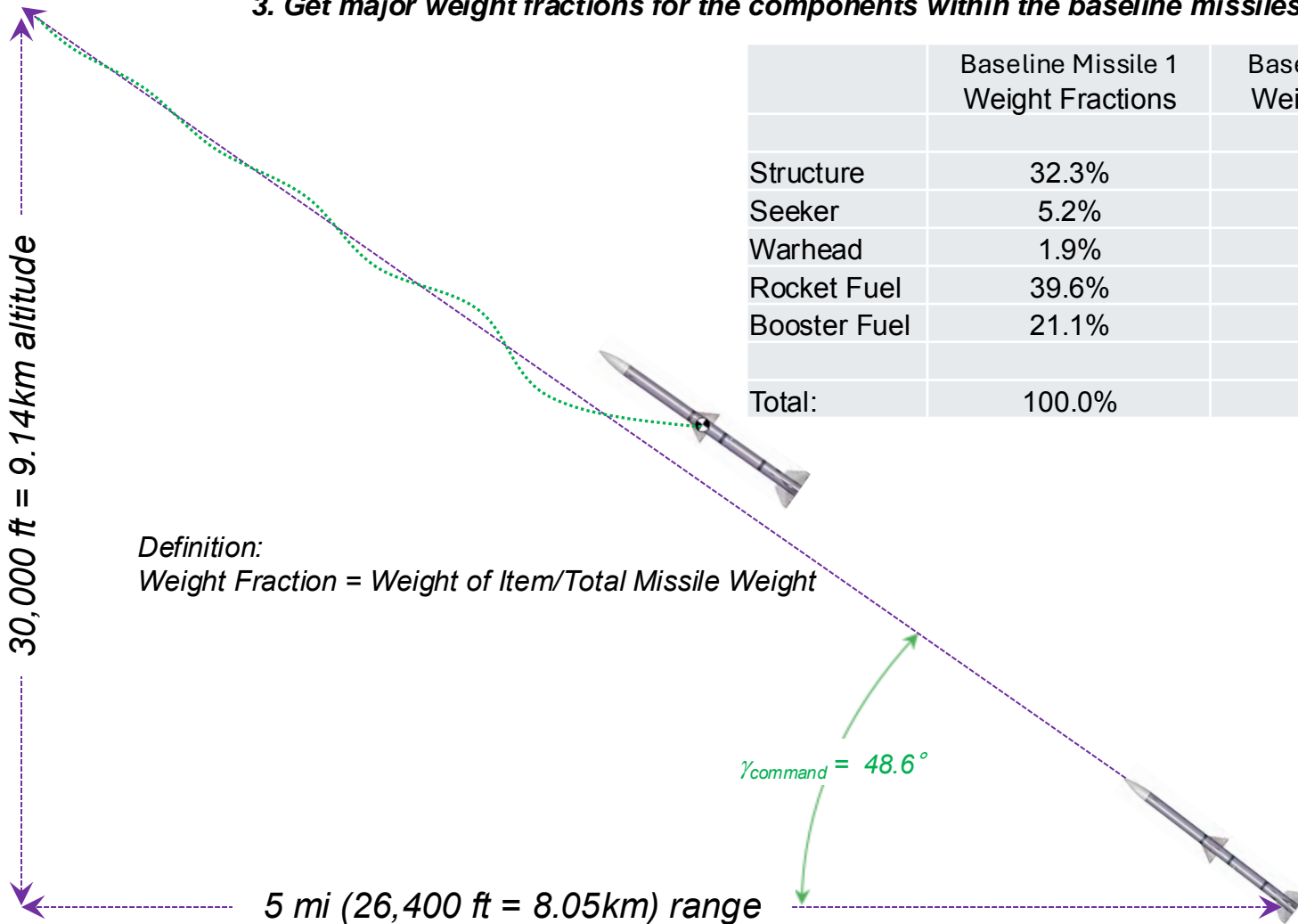
	Baseline Missile 1 Component Masses	Baseline Missile 2 Component Masses
Structure	38.2 kg	16.5 kg
Seeker	6.1 kg	3.8 kg
Warhead	2.2 kg	1.5 kg
Rocket Fuel	46.8 kg	18.3 kg
Booster Fuel	25. kg	7.2 kg
Total:	118.3 kg	47.3 kg

1st Order Proverse Engineering

Proverse design a missile to make the shot

3. Get major weight fractions for the components within the baseline missiles.

	Baseline Missile 1 Weight Fractions	Baseline Missile 2 Weight Fractions
Structure	32.3%	34.9%
Seeker	5.2%	8.0%
Warhead	1.9%	3.2%
Rocket Fuel	39.6%	38.7%
Booster Fuel	21.1%	15.2%
Total:	100.0%	100.0%



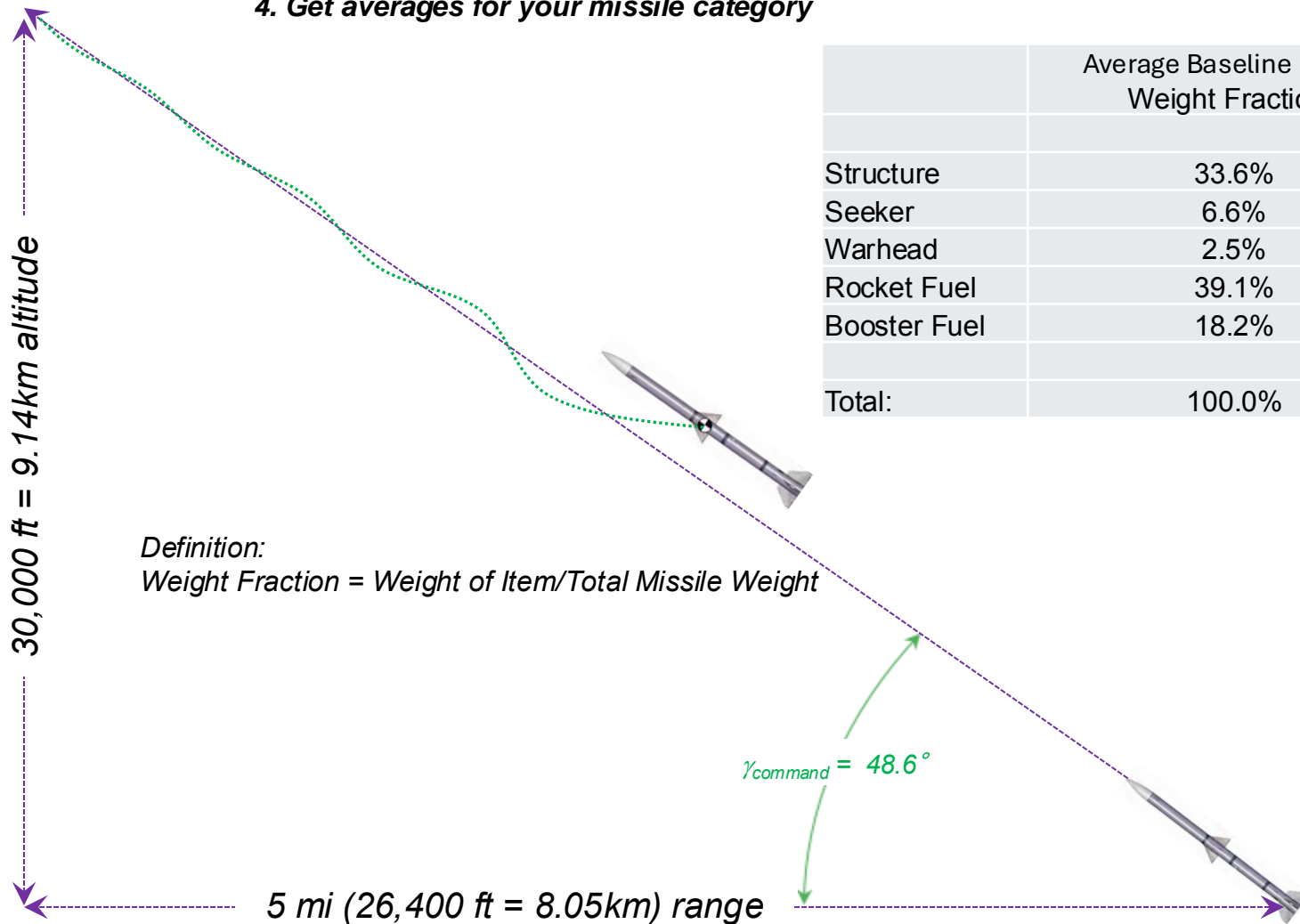
*Definition:
Weight Fraction = Weight of Item/Total Missile Weight*

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Proverse design a missile to make the shot

4. Get averages for your missile category

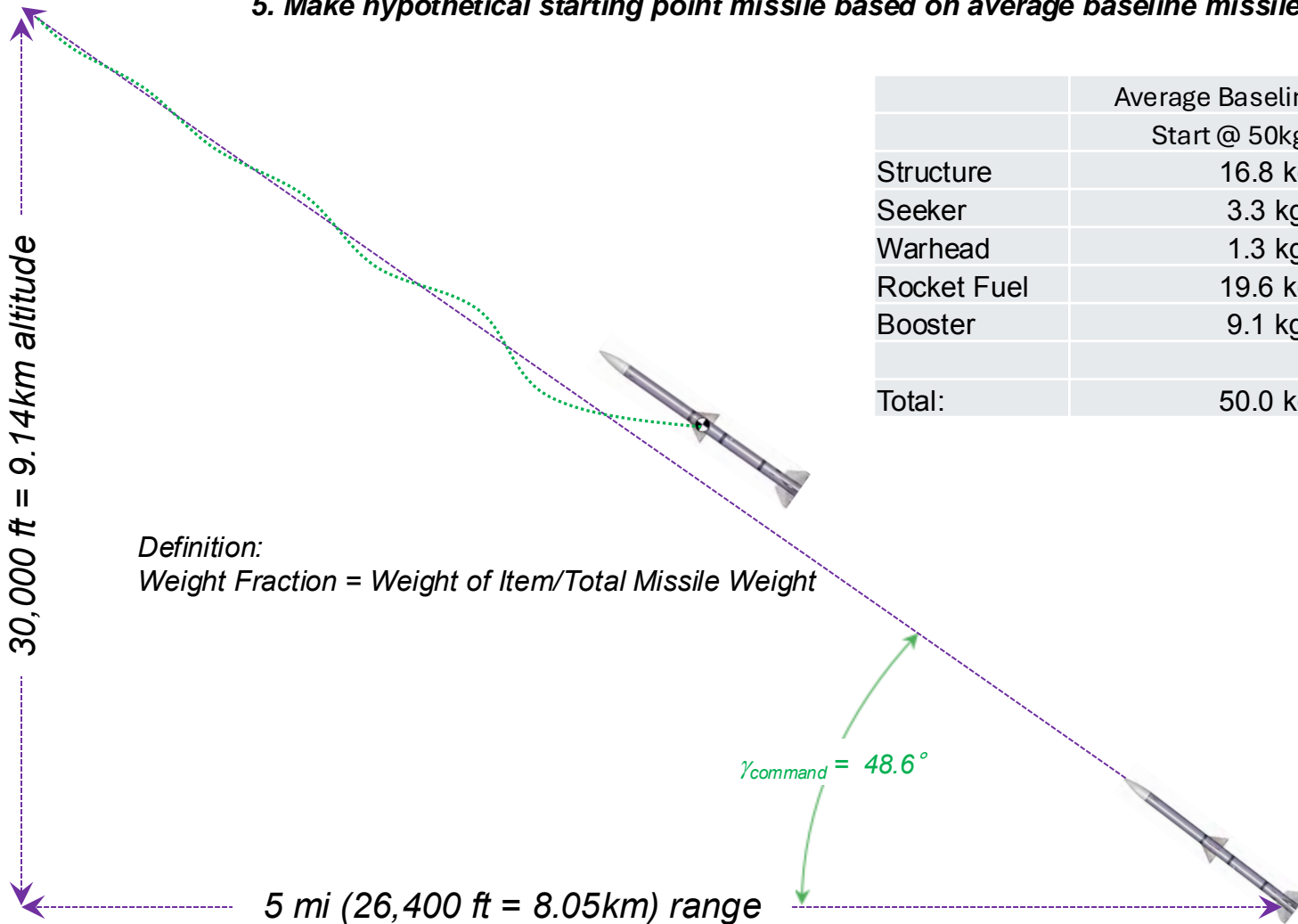
	Average Baseline Missile Weight Fractions
Structure	33.6%
Seeker	6.6%
Warhead	2.5%
Rocket Fuel	39.1%
Booster Fuel	18.2%
Total:	100.0%



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Proverse design a missile to make the shot

5. Make hypothetical starting point missile based on average baseline missile



	Average Baseline Missile
	Start @ 50kg mass
Structure	16.8 kg
Seeker	3.3 kg
Warhead	1.3 kg
Rocket Fuel	19.6 kg
Booster	9.1 kg
Total:	50.0 kg

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Proverse design a missile to make the shot

6. Assume booster imparts all of its impulse at start to get $V_{initial}$

Calculate $V_{initial}$:

Assume 1 sec. burn

$$I_{SP} = 200 \text{ sec.}$$

$$T_{impulse} = W_{booster} * I_{SP} / t_{boost}$$

$$W_{booster} = 9.81 * 9.1 \text{ kg} = 89.3 \text{ N}$$

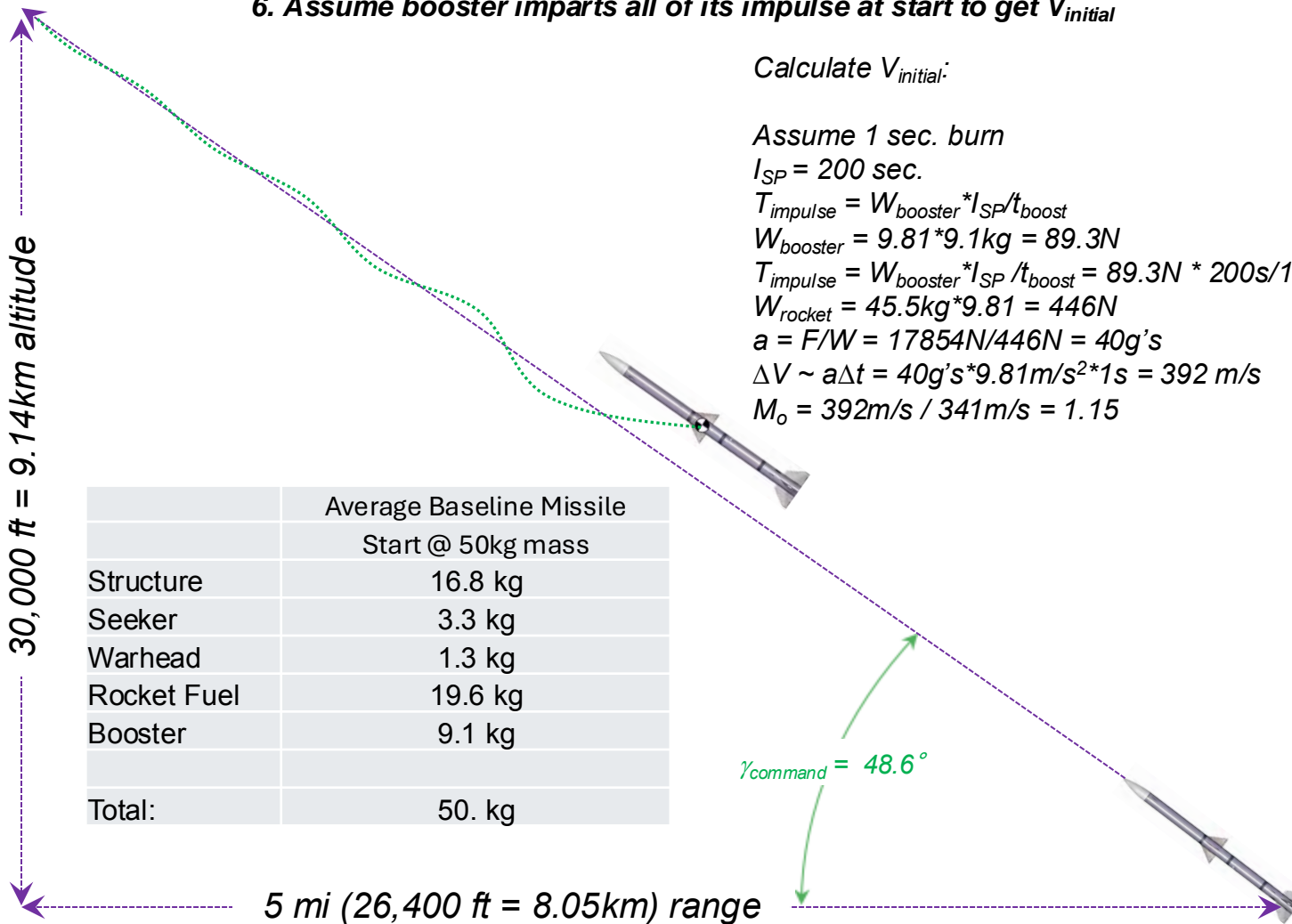
$$T_{impulse} = W_{booster} * I_{SP} / t_{boost} = 89.3 \text{ N} * 200 \text{ s} / 1 \text{ s} = 17854 \text{ N}$$

$$W_{rocket} = 45.5 \text{ kg} * 9.81 = 446 \text{ N}$$

$$a = F/W = 17854 \text{ N} / 446 \text{ N} = 40 \text{ g's}$$

$$\Delta V \sim a \Delta t = 40 \text{ g's} * 9.81 \text{ m/s}^2 * 1 \text{ s} = 392 \text{ m/s}$$

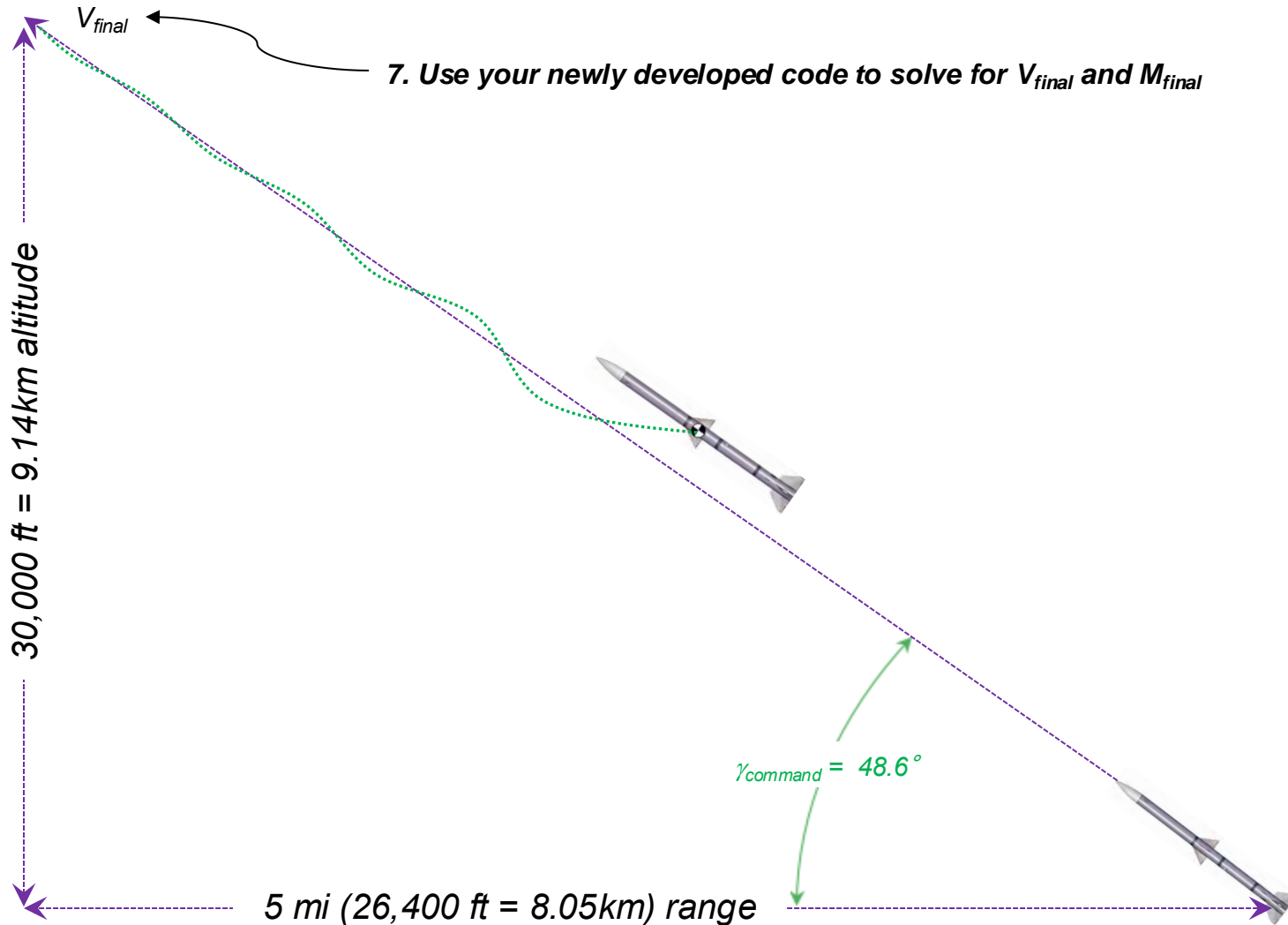
$$M_o = 392 \text{ m/s} / 341 \text{ m/s} = 1.15$$



Average Baseline Missile	
Start @ 50kg mass	
Structure	16.8 kg
Seeker	3.3 kg
Warhead	1.3 kg
Rocket Fuel	19.6 kg
Booster	9.1 kg
Total:	50. kg

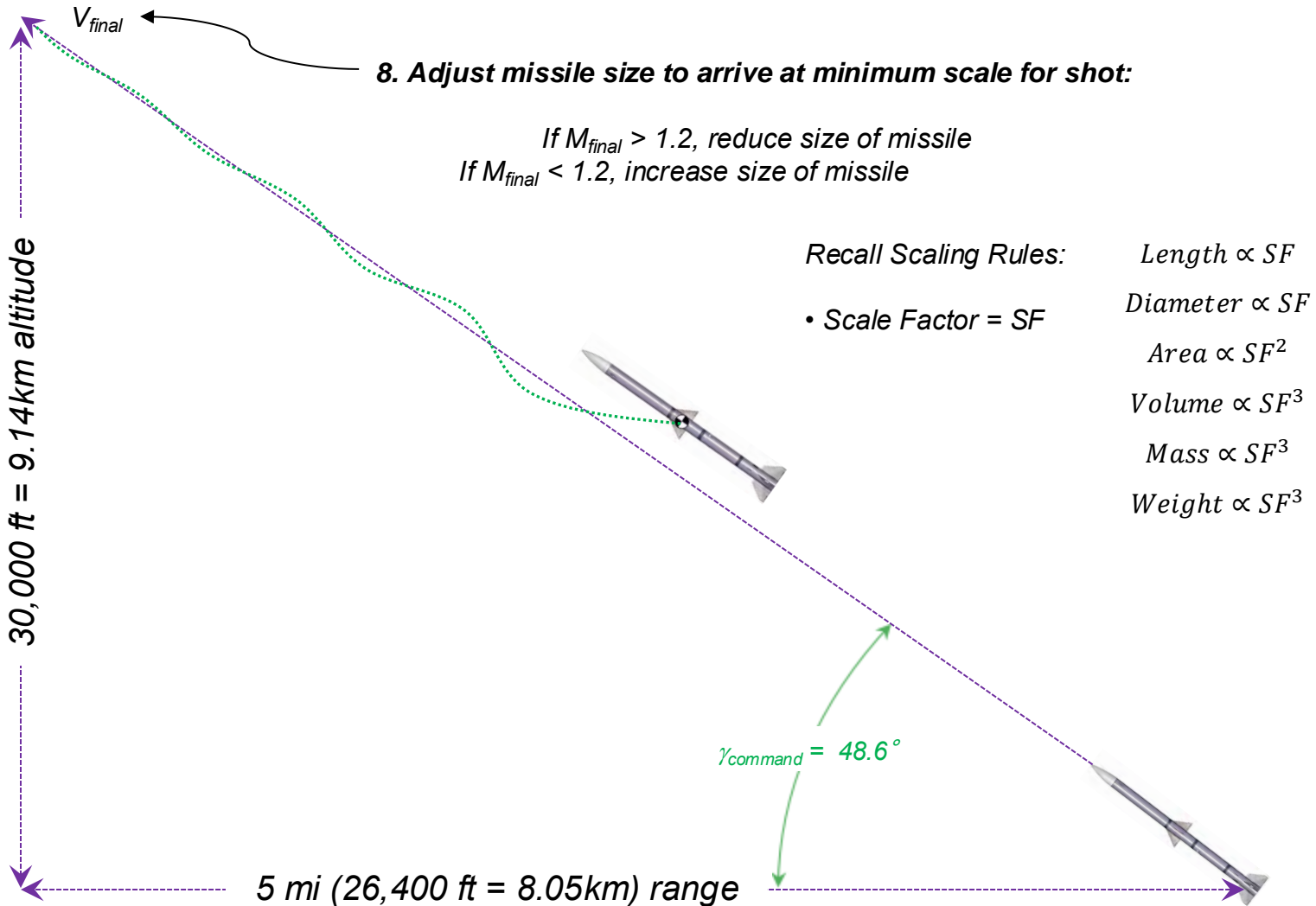
1st Order Proverse Engineering

Proverse design a missile to make the shot



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Proverse design a missile to make the shot



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Proverse design a missile to make the shot

9. Design the desired missile for the shot and CAD all components



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Proverse Design the Display Model for the Air Armament Symposium

10. Approximate Missile Dimensions for the Model

For Instance:

Sizing yields 11.9cm diameter body x 2.06m length

Call out a 5" body diameter (so we can order it)

If we can order > 72" lengths good... otherwise, set length to 72"

Scale fins proportionally



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Proverse Design the Display Model for the Air Armament Symposium

11. Assemble a Bill of Materials (BOM)

- **Part Number**
- **Name of Part**
- **Material from which part is made**
- **Quantity Required**
- **Cost per part each. and/or total**
- **Source of Part or Material**
- **Identify each part or material type on assembly view**

1st Order Proverse Engineering

Proverse Design the Display Model for the Air Armament Symposium

11. Assemble a Bill of Materials (BOM)

Part No.	Part Name & Mfg no.	Material	Qty. Rq'd	Cost per Item	Source/ Supplier	Component Weight (lb)	Weight Fraction (%)
1	Nose Cone	Fiberglass-Epoxy	1 ea.	\$32 ea	Bill's Rockets bilrock.com	1.1	4.1%
2	Forward body tube	Fiberglass-Epoxy	1 ea.	\$28 ea	Bill's Rockets bilrock.com	2.6	9.7%
3	Aft body tube	Fiberglass-Epoxy	1 ea	\$28 ea	Bill's Rockets bilrock.com	2.6	9.7%
4	Forward canards	Black aluminum	4 ea.	\$5.80 ea	Aerocomposites.com	2.4	9.0%
5	Wings	Black aluminum	4 ea.	\$6.72 ea	Aerocomposites.com	3.8	14.2%
6	Fins	Black aluminum	4 ea.	\$8.13 ea	Aerocomposites.com	5.6	21.0%
7	Launch Lugs	PLA	2 ea.	~	In-house 3d print	.38	1.4%
8	Booster rocket assembly	PLA	1 ea.	~	In-house 3d print	3.1	11.6%
9	Stand plate	Aluminum	1 ea.	\$4.60	Menards	2.3	8.6%
10	Stand flange adapter	Steel	1 ea.	\$2.95	Menards	.6	2.2%
11	Stand post	Steel	1 ea	\$3.80	Menards	2.2	8.2%
12	Sky Grey Paint	Krylon	1 ea	\$5.92	Ace Hardware	~	4.1%
13	Decals	Vinyl	1 pk	\$87.60	Decals R Us Decalsrus.com	~	9.7%
total				\$104.87		26.6 lb	

1st Order Proverse Engineering

Proverse Design the Display Model for the Air Armament Symposium

12. Start 3-D printing, Get list of components along with URLs to Dr. B. for purchase + glue, fastners etc.

Part No.	Part Name & Mfg no.	Material	Qty. Rq'd	Cost per Item	Source/ Supplier	Component Weight (lb)	Weight Fraction (%)
1	Nose Cone	Fiberglass-Epoxy	1 ea.	\$32 ea	Bill's Rockets bilrock.com	1.1	4.1%
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total				\$104.87		26.6 lb	